

22 March 2023

332 WAINUI ROAD

MILLDALE

GEOTECHNICAL COMPLETION REPORT

WFH Properties Limited

AKL2019-0182AM Rev. 1

AKL2019-0182AM				
Date	Revision	Comments		
14 December 2022	А	Initial draft for internal review		
16 December 2022	0	Final draft for client review		
22 March 2023	1	Final		

	Name	Signature	Position
Prepared by	Chris Ritchie		Associate Engineering Geologist CMEngNZ, PEngGeol
Reviewed and Authorised by	Richard Knowles	let knowle,	Principal Geotechnical Engineer CMEngNZ, CPEng



TABLE OF CONTENTS

1	INT	RODUCTION	1
2	DES	SCRIPTION OF WORKS	2
3	GEO	DTECHNICAL QUALITY CONTROL	3
	3.1 3.2	Site Observations	
4	EVA	ALUATION OF COMPLETED EARTHWORKS	3
	4.1 4.2 4.3	Natural Hazards Liquefaction	4
	4.4 4.5	Reinforced Earth Slopes	5 5
	4.6 4.7 4.8	No Build Zones	5
	4.9 <i>4.9</i> <i>4.9.</i>	Subsoil Drains and Groundwater 6 1 Underfill Drains	6 6
	<i>4.9.</i> 4.10 4.11	2 Groundwater	6
	4.11 4.11	1.1 Bearing Capacity	6 6
	4.11 4.11 4.12		8
5	CLC	DSURE	B

Using your CMW Geotechnical Report

Appendices

Appendix A: Statement of Professional Opinion on Suitability of Land for Building Construction

Appendix B: Statement of Suitability of Engineered Fill for Lightweight Structures

Appendix C: Drawings

Appendix D: Field Test Data

Appendix E: Laboratory Test Data

1 INTRODUCTION

In accordance with our instructions, this Geotechnical Completion Report has been prepared for WFH Properties Limited as part of the documentation to be submitted to Auckland Council following earthworks to form the development.

This report covers the construction period November 2021 to March 2023 and is intended to be used for certification purposes for new lots (listed below) created from SECT 15 SO 503979 as follows:

- 30 new residential lots numbered 1 to 30;
- 3 new jointly owned access lots numbered 6000 to 6002;
- 1 new accessway lot numbered Lot 7000;
- 1 new road in lot 8000 and portions of Wainui Road in Lot 8001 and Lot 8002;

The 332 Wainui Road development is located off Wainui Road, Milldale. As can be seen from the as-built plans, 27 of the lots have been affected by filling as part of the earthworks operations to a maximum depth of approximately 5.0 metres.

Construction of this subdivision has been undertaken in general accordance with;

- Auckland Council's Resource Consent number SUB60359409/LUC60359408 and Engineering Approval letter ref. ENG60382266
- Auckland Council's Building Consent BCO10342869 for cantilever timber pole retaining walls numbered Retaining Wall 01
- Auckland Council's Building Consent BCO10348690 for gabion retaining wall
- NZS4431:2022
- Auckland Council's Code of Practice for Land Development and Subdivision, Chapter 2 Earthworks and Geotechnical, Version 2.0, July 2022
- Woods consented drawing set referenced P18-276-(001-700), dated December 2020
- CMW Geosciences' Geotechnical Works Specification referenced AKL2019-0182AD, Rev. 0, dated 22 January 2020
- CMW Geosciences' Geotechnical Investigation Report referenced AKL2019-0182AB, Rev. 1, dated 27 March 2020
- CMW Geosciences' Retaining Wall Design Report referenced AKL2019-0182AG, Rev. 0, dated 2 October 2020
- CMW Geosciences' Gabion Wall Design Report referenced AKL2019-0182AH, Rev. 0, dated 21 December 2020

For the construction of these stages of the development, the following roles were fulfilled as defined in NZS 4402:2002 and the Ministry for the Environment Contaminated Land Management Guidelines:

- Geotechnical Designer: CMW Geotechnical NZ Limited
- Certifier: CMW Geotechnical NZ Limited
- Recognised Laboratory: CMW Geotechnical NZ Limited
- Contractor: March Cato Developments Ltd

As CMW has fulfilled the roles of both earth fills Certifier and Geotechnical Designer, this report has been prepared as a combined report covering both of these aspects of the project work.

2 DESCRIPTION OF WORKS

March Cato commenced work across the development in early December 2021 with earthworks operations across site. Cut material was sourced from the southern portion and placed as engineered fill across the northern area. During earthworks, unsuitable materials were encountered across site. These materials varied significantly and contained mixtures of organics, hardfill, concrete and other waste. Existing unsuitable fill was progressively undercut and stockpiled to be exported from site.

Earthworks continued through January and February 2022 which consisted of cut/fill operations with localised undercuts to remove unsuitable material. Formation of the cul-de-sac commenced which required undercuts up to 2m below existing ground levels. Utility trenching was undertaken progressively during this time as the adjacent sections of the road were undercut and remediated.

Stripping works continued throughout March 2022 as fill operations extended northwards. Lime stabilisation was used in localised areas where fill was unable to be conditioned. Alluvial material associated with the existing northern gully feature was undercut and subsoil drains were installed prior to backfilling. In late March 2022 the northern portion was stripped and prepared for the construction of the reinforced earth (RE) batter.

Construction of the RE slope along the northern boundary of site commenced in early April 2022 which involved formation of a 1.0m deep stability undercut with associated subsoil drainage and installation of geogrid between engineered fill lifts. Ongoing cut/fill operations continued throughout April and May 2022 across the rest of the site.

Earthworks operations had slowed significantly by the start of June 2022 as conditioning fill became increasingly difficult due to winter weather conditions. Attention turned to civil works around site. Installation of stormwater service lines and construction of the timber pole cantilever retaining wall commenced in early June 2022 and continued throughout the rest of the month. In mid-June 2022 the gabion outfall structure was constructed at the base of the existing northern gully.

Civil works continued through July and August 2022 with minor earthworks being undertaken where possible using lime-stabilised fill. In early August, construction of the gabion wall around the northern gully commenced which was completed in early September 2022.

Through September and October roading aggregates were laid and kerbing of Road 01 was completed. The final section of earthworks in the north-western corner of site was completed which consisted of localised undercuts of uncontrolled fill to maximum depths of 1.5m.

Throughout November and early December, lots were trimmed to final subgrade and topsoiled. Installation of the Geoweb was undertaken along the northern fill batter of Lots 18 to 22 included. A small section of Geoweb was also installed across the northern batter of Lot 17.

Works were complete by March 2023 with final topsoiling of lots, line marking on the roads and fencing.

The main items of plant used by March Cato Developments Ltd included:

- 3 x 20T Excavators;
- 1 x 13T Excavator;
- 1 x 8T Excavator;
- 1 x 5T Excavator;
- 2 x 9T Dumpers;
- 1 x Smooth Drum Roller;
- 1 x Padfoot Compactor;
- 1 x Tractor + Discs;
- 1 x Water Cart.

3 GEOTECHNICAL QUALITY CONTROL

3.1 Site Observations

During the works site visits were typically undertaken several times each week to assess compliance with NZS 4431 and project specific design recommendations and specifications.

Site visits were carried out to observe and confirm compliance relating to:

- Adequate topsoil stripping;
- Fill areas prior to the placement of fill materials to ascertain that all organic, and soft inorganic subsoils and existing, uncertified fills had been removed;
- Installation of underfill drains but excluding road under-channel drains;
- Backfilling of underfill drains;
- Excavation and backfilling of sewer and stormwater trenches;
- Subsoil drain connections to outlets and flushing at the completion of the works (yet to be completed);
- Construction of cantilever pole retaining walls including ground conditions, pile size, spacing and depth;
- Construction of gabion retaining walls including founding ground conditions, basket typology and arrangement, installation of drainage; and
- Placement and compaction of engineered fills.

3.2 Compaction Control

Compaction of engineered earth fills was controlled by undrained shear strength measured by handheld shear vane calibrated using the NZGS 2001 method and by air voids as defined by NZS4402.

General Fills

The criteria for undrained shear strength were a minimum single value of 110 kPa and minimum average of any 10 consecutive tests of 140 kPa.

The criteria for air voids were a maximum single value of 12% and maximum average of any 10 consecutive tests of 10%.

Service Line Backfills

Stormwater and wastewater lines and manhole surrounds. The criteria for undrained shear strength were a minimum average of any 10 consecutive tests of 100 kPa. The criteria for air voids were a maximum average of any 10 consecutive tests of 12%. Testing frequency was as required.

Where hardfill was used within these lines, a Clegg Impact Value of >25 was adopted.

Vane shear strength, water content and in situ density tests were carried out on all areas of the filling to at least the frequency required by the project specification.

While these tests showed on occasions that the contractor was struggling to achieve the required compaction standards with the prevailing site and soil conditions, to the best of our knowledge, all areas of fill were re-worked as necessary. Subsequent testing confirmed compliance with the specification.

4 EVALUATION OF COMPLETED EARTHWORKS

4.1 Natural Hazards

The LT Plans depict the extents of a series of zones that contain limitations intended to ensure that future building and/ or earthworks on the lots is undertaken in a manner that does not lead to buildings being subject to any of the natural hazards described in Section 71(3) of the Building Act, i.e. erosion, falling

debris, subsidence, slippage, and inundation. Consideration of the inundation hazard was outside the scope of CMW's brief and has been assessed by others. The applied zones include:

- Specific Design Zones (retaining) intended to protect the retaining walls from undermining at the toe that could lead to instability;
- Specific Design Zones (slope) intended to protect building development from long term creep effects on or adjacent to steep slopes and to protect the slopes from inappropriate loading or undermining. This zone provides a buffer between land that is suitable for NZS3604-type (Light Timber Framed Building) foundations and No Build / Planting zones.
- Specific Design Zone (Reinforced Earth Slope) intended to protect building development from long term creep effects above steep slopes and to protect the slopes from inappropriate loading. These zones also contain geogrids and geoweb anchors which should be protected from building development.
- No Build Zones (Planting Covenant) intended to protect vegetation and to ensure that stability conditions are not able to be compromised by development in areas outside the building platforms on the affected lots.

Full descriptions of the restrictions associated with each of these zones are presented in our Opinion on Suitability in *Appendix A*. Additional information is also provided in some of the following sections.

4.2 Liquefaction

The liquefaction risk for the lots on this development has been assessed as follows:

- Review of Auckland Council GIS maps confirms the damage category to be: Unlikely.
- In accordance with MBIE/NZGS guidance¹ the liquefaction susceptibility of the soils at this site was
 assessed with respect to geological age and compositional (soil fabric and density) criteria during initial
 investigations. Our assessment was described in our Geotechnical Investigation Report referenced in
 Section 1 above and found a very low risk.

4.3 Land Stability and Erosion Control

The subdivision scheme layout includes a batter slope along the northern boundary to form level terraces for building platforms. The batters are largely below the residential lots with maximum gradients of 1(v) in 2.0(h) as depicted on the as-built drawings.

Design of the works to provide appropriate stability conditions that meet regulatory requirements for the land within the development, including the batters, has led to the construction of reinforced earth (RE) slopes with associated subsoil drainage and Geoweb facing.

Stability conditions for finished ground profiles have been assessed under a range of groundwater conditions which satisfy ultimate limit state design criteria. The soil parameters for the analyses were selected from extensive investigation undertaken at the site and from experience in this terrain. We consider that the stability results are satisfactory for all building platform areas, and we are therefore satisfied that these areas are <u>not</u> subject to the natural stability hazards described in the Building Act.

On all steep land, including on engineered batter slopes, surface stability can be compromised by indiscriminate disposal of stormwater onto the ground surface and/ or by removal of vegetation.

Building and landscape designers must ensure that all runoff from solid surfaces is directed into the stormwater system. It is also important that care is paid to the disposal of stormwater during construction so that concentrated discharges (e.g. from unconnected spouting) are not directed towards steep ground.

Depths of mulch and topsoil applied to sloping areas should be limited to less than 150mm to minimise the risks of saturation leading to localised slumping on batter face. Wherever practical on such land, and

¹ Earthquake Geotechnical Engineering Practice, Module 3: Identification, assessment and mitigation of liquefaction hazards", (November 2021)

particularly on steep batters, existing vegetation and grass cover should be well maintained. Any vegetation cleared beyond the immediate area of building platforms for temporary construction purposes should be replanted or replaced as soon as possible. The roots of an established vegetation cover can serve to bind the surface soils while the foliage can reduce rain infiltration and soil saturation, resulting in better resistance to erosion and shallow slumping.

4.4 Reinforced Earth Slopes

As noted above, reinforced earth (RE) slopes have been formed with horizontal layers of geogrid embedded near the face to limit creep movement of steep slopes. Geogrids extend up to 2m behind the slope face and are buried at least 500mm from the finished surface.

The RE slopes have been finished with a cellular confinement system (Geoweb) to stabilise the topsoil on the slope faces. This system employs a series of ground anchors and tendons above the crest of the slope to keep the web in place. These are approximately 1m back from the batter face at 800mm centres.

4.5 Retaining Walls

A cantilever timber pole retaining wall has been constructed on the eastern boundaries of lots 1 and 8 in the location shown on the appended As-built Plans. The wall reaches a maximum height of approximately 2.4 metres and was designed by CMW Geosciences and the construction was observed by this consultancy.

A Gabion wall has also been constructed surrounding the stormwater outfall situated on lot 7001 in the northern portion of site, indicated on the appended A-built Plans. The wall reaches a maximum retained height of approximately 2.m and was designed by CMW Geosciences Limited.

Descriptions of the building and earthworks restrictions within the vicinity of these walls (Specific Design Zones – retaining) are contained in our Opinion on Suitability in *Appendix A*.

4.6 No Build Zones

No build / planting covenants areas have been included upslope of the lots neighbouring the northern motorway. Areas within the planting covenant contain uncertified landscape fill and steep gradients in places and have not been engineered to improve both stability conditions or the potential for load induced settlement.

4.7 Fill Induced Settlement

On the basis of the extensive undercutting of unsuitable fills, relatively minor magnitude of fill depths on this site, together with the elapsed time since it was placed, we consider that remaining post-construction settlements will be within code limits, apart from in no build areas were unsuitables were not undercut as noted in Section 4.6 above.

4.8 Service Line Trenches

As part of the civil works, sanitary sewer and stormwater services were trenched throughout the development as shown on the appended Woods Stormwater and Sanitary Sewer As-built Plans.

As is normal on all subdivisions, building developments involving foundations within a 45-degree zone of influence from pipe inverts will require engineering input. The Auckland Council drawing referenced SW22 provided in *Appendix B* extracted from Chapter 4 of the Auckland Council Code of Practice for Land development and Subdivision depicts their requirements for stormwater pipes. Details for water and wastewater pipes are available in the Watercare COP1 - General Requirements and Procedures. The majority of lots are known to have service trenches within the lots as shown on the appended stormwater and wastewater as-built plans. The resulting restrictions are presented in our Opinion on Suitability in *Appendix A*.

4.9 Subsoil Drains and Groundwater

The appended Woods as-built plan shows the positions of subsoil drains and their outlets that were installed during the earthworks as described in the following sub-sections.

Descriptions of restrictions associated with these drains and outlets are contained in our appended Opinion on Suitability in *Appendix A*.

4.9.1 Underfill Drains

These drains were installed at the bases of fills to assist with the earthworks operations by capturing seepages at the cleared ground level. They require no specific maintenance and while their ongoing function is not critical to stability conditions, but they provide ongoing control of groundwater levels and pore water pressure relief so their ongoing function should not be compromised by future works.

Typically these drains comprise punched draincoils surrounded by drainage gravel. Specific design details are provided in the project reports and specifications. If drain depths are unclear at specific locations, they can be estimated from the depths of fills depicted on the as-built plans.

4.9.2 Groundwater

Groundwater levels beneath the engineered fills can be expected to be controlled by the underfill drains and should therefore typically be deeper than 2m, subject to seasonal variations.

In areas of natural ground, based on our work to date we anticipate groundwater levels remaining well below the depth of influence of anticipated earthworks and foundation works for NZS 3604 type dwellings.

4.10 Road Subgrades

Penetration resistance testing was carried out on the road subgrades during construction and the results of this testing were forwarded to Woods Limited for pavement remedial design. Where soft ground with low equivalent CBR values was identified it was generally undercut and replaced with engineered fill. All road subgrade areas were subsequently lime/ cement stabilised to achieve appropriate CBR values.

4.11 Design of Shallow Foundations

4.11.1 Bearing Capacity

Once bulk earthworks and top-soiling of the building platforms had been completed, our staff drilled hand auger boreholes on platforms in natural ground to determine representative finished ground conditions and hence evaluate likely foundation options for future building development. Our assessments of bearing capacity for the design of shallow foundations on each building platform are contained in our Opinion on Suitability in *Appendix A.*

As also detailed in our Opinion on Suitability, some lots in natural (cut) ground have lower bearing capacities than the 300kPa required by the definition of NZS 3604 "good ground". However, this will not necessarily alter the form or cost of foundations on these lots, depending on development proposals.

If higher geotechnical ultimate bearing capacities are required than have been specified, further specific site investigation and design of foundations should be carried out prior to Building Consent application.

4.11.2Foundation Settlements

At the bearing pressures specified above and subject to the design requirements for soil expansiveness provided below, differential settlement of shallow foundations for buildings designed in accordance with NZS 3604 (including the 600mm subfloor fill depth limit) should be within code limits.

4.11.3Soil Expansiveness Classification

Seasonal shrinking and swelling results in vertical surface ground movement which can cause significant cracking of floor slabs and walls. NZS 3604:2011² excludes from the definition of 'good ground', soils with a liquid limit of more than 50% and a linear shrinkage of more than 15% due to their potential to shrink and swell as a result of seasonal fluctuations in water content. For soils exceeding these limits, NZS 3604 has historically referenced AS 2870³. for foundation design advice. However, the November 2019 update of Acceptable Solution B1/AS1⁴ provides amendments to NZS 3604 that define a method for testing and classifying the soils and provides foundation designs for specific, simple house configurations across the range of expansive soil conditions.

Nevertheless, there is evidence⁵ indicating that the use of the B1/AS1 method of assessment of expansiveness may be inaccurate.

Testing of samples obtained from the site was carried out by Road Test, an IANZ registered Testing Authority to provide the geotechnical parameters required for our assessment as presented in Table 1.

Table 1: Soil Expans	siveness Testing Schedule	
Type of Test	Test Method	Quantity
Water Content	NZS4402 – 1986 2.1	4
Liquid Limit	NZS4402 – 1986 2.2	4
Linear shrinkage	NZS4402 – 1986 2.6	4

Certificates for the test results outlined above are presented in Appendix F.

Test results were used in conjunction with visual-tactile assessment of the site soils and BRANZ Report SR120A⁶ to determine expansive site Classes as defined in AS 2870, "Residential Slabs and Footings – Construction". Resulting classifications are provided in the Statement of Suitability in *Appendix A*.

The expansive soil hazard is addressed by a combination of design that is appropriate for the expansive Class described in our Opinion on Suitability in *Appendix A*, together with care during site preparation for foundations and diligent maintenance of plantings near the foundations.

Site Preparation

There have been many instances of concrete floors and/ or foundations that have been poured on dry, desiccated subgrades in summer months on expansive soils and have undergone heaving and cracking requiring extensive repairs or even complete house re-builds once the soil moisture contents have returned to higher levels. In some instances, perimeter foundations have been appropriately treated but floor slabs have been poured on dry ground. Infiltration of moisture via pipe bedding has then occurred.

Foundation contractors need to be made aware of the extreme damage potentially caused by these circumstances and the need to maintain appropriate moisture contents in both the footings <u>and</u> building platform subgrade between the time of excavation and the pouring of concrete.

Remedial actions that may be appropriate include combinations of platform protection with a hard fill layer, pouring of a blinding layer of concrete in footing bases and soaking of the building platform with sprinklers for an extended period.

² Standards New Zealand (2011) Timber-framed buildings, NZS 3604:2011, NZ Standard

³ Standards Australia Limited (2011) Residential slabs and footings, AS 2870-2011, Australian Standard, NSW

⁴ Ministry of Business, Innovation and Employment (2019) Acceptable Solutions and Verification Methods for NZ Building Code Clause B1 Structure, B1/AS1, Amendment 19

⁵ Rogers, N., McDougall, N., Twose, G., Teal, J. & Smith, T. (2020) The Shrink Swell Test: A Critical Analysis, *NZ Geomechanics News*, Issue 99, pages 66-80.

⁶ Fraser Thomas Limited (2008) - Addendum Study Report (BRANZ SR120A), Soil Expansivity in the Auckland Region – Final Report

Site Maintenance

Landowners must be mindful that either the <u>planting or removal</u> of high water demand plants where their roots may extend close to footings (i.e. within a lateral distance of 1.5 times the mature tree height) can cause settlement or heave damage.

4.11.4Site (Seismic) Class

Our assessments of NZS 1170.5 site Class(es) is provided in our Opinion of Suitability and the Summary Table, both in *Appendix A*.

4.12 Topsoil Depths

Topsoil depths have been checked by the drilling of a borehole in the approximate centre of the building platform on a representative sample of lots. The results are considered indicative for each lot, but may be subject to variations. Topsoil depths were found to be between 20 and 220mm on this stage of the development.

Site specific findings are contained in the appended Suitability Statement Summary (*Appendix A*). However, it is possible that further levelling works have been undertaken since our investigations and accordingly, we strongly recommend that lot purchasers complete their own checks of topsoil depths.

5 CLOSURE

Additional important information regarding the use of your CMW report is provided in the 'Using your CMW Report' document attached to this report.

This report has been prepared for use by WFH Properties Limited in relation to the 332 Wainui Road Milldale project in accordance with the scope, proposed uses and limitations described in the report. Should you have further questions relating to the use of your report please do not hesitate to contact us.

Although regular site visits have been undertaken for observation, for providing guidance and instruction and for testing purposes, the geotechnical services scope did not include full time site presence. To this end, our Opinion on Suitability in *Appendix A* and our Suitability Statement in *Appendix B* also rely on the Contractors' work practices and assumes that when we have not been present to observe the work, it has been completed to high standards and in accordance with the drawings, instructions and consent conditions provided to them.

Similarly, they assume that all as-built information and other details provided to the Client and/ or CMW by other members of the project team are accurate and correct in all respects.

Where a party other than WFH Properties Limited seeks to rely upon or otherwise use this report, the consent of CMW should be sought prior to any such use. CMW can then advise whether the report and its contents are suitable for the intended use by the other party.



USING YOUR CMW GEOTECHNICAL REPORT

Geotechnical reporting relies on interpretation of facts and collected information using experience, professional judgement, and opinion. As such it generally has a level of uncertainty attached to it, which is often far less exact than other engineering design disciplines. The notes below provide general advice on what can be reasonably expected from your report and the inherent limitations of a geotechnical report.

Preparation of your report

Your geotechnical report has been written for your use on your project. The contents of your report may not meet the needs of others who may have different objectives or requirements. The report has been prepared using generally accepted Geotechnical Engineering and Engineering Geology practices and procedures. The opinions and conclusions reached in your report are made in accordance with these accepted principles. Specific items of geotechnical or geological importance are highlighted in the report.

In producing your report, we have relied on the information which is referenced or summarised in the report. If further information becomes available or the nature of your project changes, then the findings in this report may no longer be appropriate. In such cases the report must be reviewed, and any necessary changes must be made by us.

Your geotechnical report is based on your project's requirements

Your geotechnical report has been developed based on your specific project requirements and only applies to the site in this report. Project requirements could include the type of works being undertaken; project locality, size and configuration; the location of any structures on or around the site; the presence of underground utilities; proposed design methodology; the duration or design life of the works; and construction method and/or sequencing.

The information or advice in your geotechnical report should not be applied to any other project given the intrinsic differences between different projects and site locations. Similarly geotechnical information, data and conclusions from other sites and projects may not be relevant or appropriate for your project.

Interpretation of geotechnical data

Site investigations identify subsurface conditions at discrete locations. Additional geotechnical information (e.g. literature and external data source review, laboratory testing etc) are interpreted by Geologists or Engineers to provide an opinion about a site specific ground models, their likely impact on the proposed development and recommended actions. Actual conditions may differ from those inferred to exist due to the variability of geological environments. The actual interface between materials may be far more gradual or abrupt than assumed based on the facts obtained. Nothing can be done to change the actual site conditions which exist, but steps can be taken to reduce the impact of unexpected conditions. Interpretation of factual data can be influenced by design and/or construction methods. Where these methods change review of the interpretation in the report may be required.

Subsurface conditions can change

Subsurface conditions are created by natural processes and then can be altered anthropically or over time. For example, groundwater levels can vary with time or activities adjacent to your site, fill may be placed on a site, or the consistency of near surface conditions might be susceptible to seasonal changes. The report is based on conditions which existed at the time of investigation. It is important to confirm whether conditions may have changed, particularly when large periods of time have elapsed since the investigations were performed.

Interpretation and use by other design professionals

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a geotechnical report. To help avoid misinterpretations, it is important to retain the assistance of CMW to work with other project design professionals who are affected by the contents of your report. CMW staff can explain the report implications to design professionals and then review design plans and specifications to see that they have correctly incorporated the findings of this report.

Your report's recommendations require confirmation during construction

Your report is based on site conditions as revealed through selective point sampling. Engineering judgement is then applied to assess how indicative of actual conditions throughout an area the point sampling might be. Any assumptions made cannot be substantiated until construction is complete. For this reason, you should retain geotechnical services throughout the construction stage, to identify variances from previous assumption, conduct additional tests if required and recommend solutions to problems encountered on site.

A Geotechnical Engineer, who is fully familiar with the site and the background information, can assess whether the report's recommendations remain valid and whether changes should be considered as the project develops. An unfamiliar party using this report increases the risk that the report will be misinterpreted.

Environmental Matters Are Not Covered

Unless specifically discussed in your report environmental matters are not covered by a CMW Geotechnical Report. Environmental matters might include the level of contaminants present of the site covered by this report, potential uses or treatment of contaminated materials or the disposal of contaminated materials. These matters can be complex and are often governed by specific legislation.

The personnel, equipment, and techniques used to perform an environmental study can differ significantly from those used in this report. For that reason, our report does not provide environmental recommendations. Unanticipated subsurface environmental problems can have large consequences for your site. If you have not obtained your own environmental information about the project site, ask your CMW contact about how to find environmental risk-management guidance.

Appendix A: Statement of Professional Opinion on Suitability of Land for Building Construction

STATEMENT OF PROFESSIONAL OPINION ON SUITABILITY OF LAND FOR BUILDING CONSTRUCTION

Development:	332 Wainui Road Subdivision Development
Developer:	WFH Properties Limited
Location:	Milldale

I, Chris Ritchie, of CMW Geotechnical NZ Limited, Auckland, hereby confirm that:

- 1. As a Chartered Engineering Geologist experienced in the field of geotechnical engineering, I am a Geo-professional as defined in clause 1.2.2 of NZS 4404:2010 and was retained by the Developer as the geo-professional on the above development.
- 2. The extent of preliminary investigations carried out to date are described in the CMW Geosciences Geotechnical Investigation Report referenced AKL2019-0182AB Rev. 1, dated 27 March 2020. The conclusions and recommendations of this document have been re-evaluated in the preparation of this report. The extent of my inspections during construction, and the results of all tests and/ or evaluations carried out are as described in my Geotechnical Completion Report dated 22 March 2023.
- 3. My certification of the earth fills placed on this site is contained in Appendix B.
- 4. In my professional opinion, not to be construed as a guarantee, I consider that:
 - (a) The completed earthworks take into account land slope and foundation stability considerations on the building platform areas, but as shown on the appended as built plans, areas on Lots 8 to 16 have gradients steeper (or directly above) than 1(v) in 4(h) (and generally up to 1(v) in 2(h)). Accordingly, restrictions incorporating **Specific Design Zones (Slope)** have been applied directly below the No Build / Land Covenant Zone on Lots 8 to 16 inclusive as depicted on the LT Plans.

No building construction <u>and</u> no cuts of any depth should take place within the designated **Specific Design Zone (Slope) areas** unless endorsed by a Chartered Professional Engineer experienced in geomechanics and familiar with the contents of this report. The endorsement will need to consider the implications of the proposals on the global stability of the Northern Motorway batter.

This limitation also applies to long term landscaping works, including any proposed minor cuts either on or near batter toes to be retained by new landscaping walls that might not normally require engineering, and to landscaping fills on or immediately above the batter slopes.

(b) Specific Design Zone (Reinforced Earth Slope) areas have been applied to Lots 17 to 22 as encompassing or directly above reinforced earth slopes. No building construction and no earthworks (i.e. cut or fills of any depth) should take place within the designated Specific Design Zone (Reinforced Earth Slope) areas unless endorsed by a Chartered Professional Engineer experienced in geomechanics and familiar with the contents of this report. The endorsement will need to consider the implications of the proposals on the global stability of the slope, soil creep on the buildings, foundations and retaining walls.

The geogrids associated with the reinforced earth slope are not expected to be encountered by development on these lots. However, should any geogrids be exposed or damaged, the work must be observed and certified by a Chartered Professional Engineer experienced in geomechanics and familiar with the contents of this report. Geoweb anchors may be encountered if excavations are carried out within 1m of the crest of these slopes. Should these be exposed or damaged, the work must be observed and certified by a Chartered Professional Engineer experienced in geomechanics are carried out within 1m of the crest of these slopes. Should these be exposed or damaged, the work must be observed and certified by a Chartered Professional Engineer experienced in geomechanics and familiar with the contents of this report.

This limitation also applies to long-term landscaping works, including landscaping fills on or immediately above the batter slopes

- (c) **Specific Design Zone (Retaining) areas** have been applied on Lots 1 and 8 for the protection of the function of the retaining walls as depicted on the as-built plans. The retaining walls on this stage of the development were designed for:
 - A maximum of 0 kPa surcharge load and 0° toe slope for Case 1 walls (Lots 1 and 8), and;
 - A maximum of 0 kPa surcharge load and 5° toe slope for Case 2 walls (Lot 8).

No building construction <u>and</u> no earthworks (i.e. cut or fills) should take place within these Specific Design Zones that exceed these design limits on the walls unless endorsed by a Chartered Professional Engineer experienced in geomechanics and familiar with the contents of this report who consider the stability implications of the earthworks and/ or building proposals on the retaining walls.

(d) **No Build / Land Covenant Zone** areas defined on Lots 8-16 inclusive are designated no-build zones on the basis of potential for instability and/ or because of the presence of planting areas.

No building construction and no earthworks may take place in these areas.

- (e) The function of the subsoil drains installed beneath Lots 18 to 23 and 30 inclusive as shown on the as-built plans must not be impaired by any building development or landscaping works. Any bored or driven piles must be positioned to avoid damaging the draincoils. Where any subsoil drain is intercepted by building works, it must be reinstated under the direction of a Chartered Professional Engineer to ensure the integrity of the subsoil drainage system.
- (f) A geotechnical ultimate bearing capacity of 300 kPa may be assumed for shallow foundation design on the building platforms of Lots 1 to 30 inclusive.

If for any reason higher geotechnical bearing capacities are required, further specific site investigation and design of foundations should be carried out prior to Building Consent application.

- (g) The site (seismic) subsoil class for each lot has been assessed in accordance with NZS1170.5:2004 Clause 3.1.3 from borelogs that included measurements of geotechnical properties. Our assessment is that all lots are Class C- shallow soil.
- (h) The expansive site Class for all lots has been assessed as AS2870 Class M (Moderate) to H1 (Highly). We recommend that building designers note on the Building Consent drawings the need to maintain appropriate moisture levels across building subgrades and in footing excavations (as described in Section 4.11.3 of the Geotechnical Completion Report) for reference by foundation contractors.
- (i) No building development should take place within the 45 degree zone of influence of stormwater or sewer line or manhole inverts unless endorsed by specific design and by construction inspections undertaken by a Chartered Professional Engineer experienced in geomechanics to ensure that lateral stability and differential settlement issues are addressed and that building loads are transferred beyond the influence of pipes and trench backfills. A copy of drawing SW22 extracted from Chapter 4 of the Auckland Council Code of Practice for Land development and Subdivision this document is provided in *Appendix B* for clarification. Details for water and wastewater pipes are available in the Watercare COP1 - General Requirements and Procedures.

- (j) On the basis of the earth fill certification and subject to the geotechnical limitations, restrictions and recommendations contained in clauses 4(a), 4(b), 4(c), 4(d), 4(e), 4(f), 4(g), 4(h) and 4(i) above:
 - (i) The filled and natural ground is generally suitable for residential buildings constructed in accordance with NZS 3604 and the requirements of AS2870 for the appropriate expansive soil class.
 - (ii) Where shallow foundations are appropriate, design may be carried out in accordance with AS 2870 (Class M to H2 as specified for each lot) or alternately, a specific foundation and structural design may be undertaken by a Chartered Professional Engineer.
- 5. Road subgrades have been formed with appropriate regard for slope stability and settlement risks.
- 6. The esplanade reserve area in Lot 7001 has been formed with appropriate regard for slope stability risks.

The following table summarises the conditions on each of the residential lots.

For and on behalf of CMW Geosciences

Chris Ritchie Associate Engineering Geologist CMEngNZ, PEngGeol

			Table 2: G	CR Summar	y Table					
Condition	Specific Design Zone (Slope) – Geotechnical Land Covenant Area (refer LT Plans)	Specific Design Zone (Reinforced Slope) – Geotechnical Land Covenant Area (refer LT Plans)	Specific Design Zone (Retaining) – Geotechnical Land Covenant Area (refer LT Plans)	No Built Zone – Land Covenant Area (refer to LT Plan)	Subsoil Drains Present	Geotechnical Ultimate Bearing Capacity (kPa)	NZS 1170.5 Site (seismic) Class	AS2870 Expansive Class	Service Lines Restrictions	Indicative Topsoil Depth (mm)
GCR SOPO Clause	4(a)	4(b)	4(c)	4(d)	4(e)	4(f)	4(g)	4(h)	4(i)	
Lot number										
1			F			300	С	H1		220
2						300	С	H1		220
3						300	С	H1		20
4						300	С	H1		20
5						300	С	H1		60
6						300	С	H1		60
7						300	С	H1		200
8			G	Q		300	С	H1		150
9	Н			R		300	С	H1		150
10	I			S		300	С	H1		120
11	J			Т		300	С	H1	•	120
12	К			U		300	С	H1	•	130
13	L			V		300	С	H1	•	130
14	М			W		300	С	H1	•	70
15	Ν			Х		300	С	H1	•	70
16	0			Y		300	С	H1	•	90
17		BA				300	С	H1	•	90
18		BB			•	300	С	М		90
19		BC			•	300	С	М	•	110
20		BD			•	300	С	М	•	110

Table 2: GCR Summary Table										
Condition	Specific Design Zone (Slope) – Geotechnical Land Covenant Area (refer LT Plans)	Specific Design Zone (Reinforced Slope) – Geotechnical Land Covenant Area (refer LT Plans)	Specific Design Zone (Retaining) – Geotechnical Land Covenant Area (refer LT Plans)	No Built Zone – Land Covenant Area (refer to LT Plan)	Subsoil Drains Present	Geotechnical Ultimate Bearing Capacity (kPa)	NZS 1170.5 Site (seismic) Class	AS2870 Expansive Class	Service Lines Restrictions	Indicative Topsoil Depth (mm)
GCR SOPO Clause	4(a)	4(b)	4(c)	4(d)	4(e)	4(f)	4(g)	4(h)	4(i)	
21		BE			•	300	С	М	•	100
22		BF			•	300	С	М	•	100
23						300	С	H1	•	90
24						300	С	H1	•	90
25						300	С	H1		100
26						300	С	H1	•	100
27						300	С	H1		100
28						300	С	H1		180
29						300	С	H1		200
30					•	300	С	H1		200

Appendix B: Statement of Suitability of Engineered Fill for Lightweight Structures

STATEMENT OF SUITABILITY OF ENGINEERED FILLS FOR LIGHTWEIGHT STRUCTURES

То:	Auckland Council
Development:	332 Wainui Road Development
Land Title(s):	SECT 15 SO 503979
Location:	332 Wainui Road, Upper Orewa
Resource Consent Nos:	LUC60359408
Developer:	WFH Properties Limited
Geotechnical Designer:	Chris Ritchie of CMW Geotechnical NZ Limited
Certifier:	Chris Ritchie of CMW Geotechnical NZ Limited

This Statement of Suitability is provided as an appendix to the CMW Geosciences Geotechnical Completion Report referenced in the page footer below, that also contains all as-built plans, geotechnical works specification, test results and test inspection records relevant to the work completed.

- 1. I, Chris Ritchie, confirm that I am qualified as a certifier as defined in NZS4431:2022.
- 2. During this work, I was retained as certifier and I or my certifier's representative undertook inspections and testing as documented in the Geotechnical Completion Report.
- 3. I am satisfied that the engineered fill shown in the attached as-built survey was placed, compacted and tested in accordance with the attached specification and that all variations and non-compliances have been documented in the Geotechnical Completion report.
- 4. Based on the information available, I certify that, to the best of my knowledge, the intent of the geotechnical designer (as presented in the design, drawings and Geotechnical Works Specification) has been achieved.
- 5. This certification does not remove the necessity for normal inspection and design of foundations as would be made in natural ground.

For and on behalf of CMW Geosciences

 $\langle -$

Chris Ritchie Associate Engineering Geologist CMEngNZ, PEngGeol

Appendix C: Drawings

Title	Reference No.	Date	Revision
Draft Title Plan	LT 581992	23/02/2023	
Woods – Final Subgrade Surface Asbuilt Plan	P18-276-00-1000-AB	17/03/2023	2
Woods – Cut and Fill Asbuilt Plan (Sheets 1-3)	P18-276-00-1110-AB	17/03/2023	2
Woods – Timber Retaining Wall Asbuilt Plan	P18-276-00-1300-AB	21/03/2023	2
Woods – Gabion Retaining Wall Asbuilt Plan	P18-276-00-1301-AB	21/03/2023	1
Woods – Subsoil Asbuilt Plan	P18-276-1200-AB	21/03/2023	1
Woods – Remediated Areas	P18-276-1400-AB	24/02/2023	1
Woods – Stormwater Asbuilt Plan (Sheets 1 – 4)	P18-276-3000-AB	21/03/2023	1
Woods – Wastewater Asbuilt Plan (Sheets 1 - 3)	P18-276-4000-AB	21/03/2023	1
Auckland Council SW Pipe & MH Construction Clearance Requirements	SW22	1/11/2015	2





Title Plan - LT 581992

Survey Number	LT 581992
Surveyor Reference	P18-276 - 332 Wainui Road
Surveyor	Jessica Deborah Smyth
Survey Firm	Wood & Partners Consultants Ltd
Surveyor Declaration	

Survey Details

 Dataset Description
 Lot 1 to 30, 6000 to 6002, 7000, 7001, 8000 and 8002 Being a Subdivision of Section 15 SO 503979

 Status
 Initiated

 Land District
 North Auckland
 Survey Class
 Class A

 Submitted Date
 Exposit Date
 Deposit Date

Territorial Authorities

Auckland Council

Comprised In

RT 813338

Created Parcels

Lot 1 Deposited Plan 581992
Lot 2 Deposited Plan 581992
Lot 3 Deposited Plan 581992
Lot 4 Deposited Plan 581992
Lot 5 Deposited Plan 581992
Lot 6 Deposited Plan 581992
Lot 7 Deposited Plan 581992
Lot 8 Deposited Plan 581992
Lot 9 Deposited Plan 581992
Lot 10 Deposited Plan 581992
Lot 11 Deposited Plan 581992
Lot 12 Deposited Plan 581992
Lot 13 Deposited Plan 581992
Lot 16 Deposited Plan 581992
Lot 17 Deposited Plan 581992
Lot 18 Deposited Plan 581992
Lot 19 Deposited Plan 581992
Lot 20 Deposited Plan 581992
Lot 21 Deposited Plan 581992
Lot 22 Deposited Plan 581992
Lot 23 Deposited Plan 581992
-
Lot 24 Deposited Plan 581992
Lot 25 Deposited Plan 581992

Parcel Intent	Area	RT Reference
Fee Simple Title	0.1152 Ha	1088307
Fee Simple Title	0.0549 Ha	1088308
Fee Simple Title	0.0550 Ha	1088309
Fee Simple Title	0.0549 Ha	1088310
Fee Simple Title	0.0550 Ha	1088311
Fee Simple Title	0.0549 Ha	1088312
Fee Simple Title	0.0549 Ha	1088313
Fee Simple Title	0.0847 Ha	1088314
Fee Simple Title	0.0582 Ha	1088315
Fee Simple Title	0.0735 Ha	1088316
Fee Simple Title	0.0737 Ha	1088317
Fee Simple Title	0.0579 Ha	1088318
Fee Simple Title	0.0512 Ha	1088319
Fee Simple Title	0.0546 Ha	1088322
Fee Simple Title	0.0557 Ha	1088323
Fee Simple Title	0.0541 Ha	1088324
Fee Simple Title	0.0481 Ha	1088325
Fee Simple Title	0.0519 Ha	1088326
Fee Simple Title	0.0500 Ha	1088327
Fee Simple Title	0.0556 Ha	1088328
Fee Simple Title	0.0537 Ha	1088329
Fee Simple Title	0.0600 Ha	1088330
Fee Simple Title	0.0550 Ha	1088331





Title Plan - LT 581992

Created Parcels

Parcels

Lot 26 Deposited Plan 581992 Lot 27 Deposited Plan 581992 Lot 28 Deposited Plan 581992 Lot 29 Deposited Plan 581992 Lot 30 Deposited Plan 581992 Lot 6000 Deposited Plan 581992 Lot 6001 Deposited Plan 581992 Lot 6002 Deposited Plan 581992 Lot 7001 Deposited Plan 581992 Lot 7000 Deposited Plan 581992

Lot 8000 Deposited Plan 581992

Lot 8001 Deposited Plan 581992

Lot 8002 Deposited Plan 581992

Lot 14 Deposited Plan 581992 Lot 15 Deposited Plan 581992 Area B Deposited Plan 581992 Area C Deposited Plan 581992 Area DA Deposited Plan 581992 Area EA Deposited Plan 581992 Area F Deposited Plan 581992 Area G Deposited Plan 581992 Area H Deposited Plan 581992 Area I Deposited Plan 581992 Area J Deposited Plan 581992 Area K Deposited Plan 581992 Area L Deposited Plan 581992 Area M Deposited Plan 581992 Area N Deposited Plan 581992 Area O Deposited Plan 581992 Area Q Deposited Plan 581992 Area R Deposited Plan 581992 Area S Deposited Plan 581992 Area T Deposited Plan 581992 Area U Deposited Plan 581992 Area V Deposited Plan 581992 Area W Deposited Plan 581992 Area X Deposited Plan 581992 Area DC Deposited Plan 581992 Area Y Deposited Plan 581992 Area DB Deposited Plan 581992

Parcel Intent	Area	RT Reference
Fee Simple Title	0.0511 Ha	1088332
Fee Simple Title	0.0525 Ha	1088333
Fee Simple Title	0.0775 Ha	1088334
Fee Simple Title	0.0500 Ha	1088335
Fee Simple Title	0.0499 Ha	1088336
Fee Simple Title	0.0696 Ha	Multiple
Fee Simple Title	0.0358 Ha	Multiple
Fee Simple Title	0.0136 Ha	Multiple
Fee Simple Title	0.2028 Ha	1088337
Vesting on Deposit for	0.0215 Ha	
Accessway		
Vesting on Deposit for Road	0.3110 Ha	
Vesting on Deposit for Road	0.0192 Ha	
Vesting on Deposit for	0.0762 Ha	
Road	0.070211a	
Fee Simple Title	0.0504 Ha	1088320
Fee Simple Title	0.0633 Ha	1088321
Easement		
Covenant - Land		

Covenant - Land Easement Covenant - Land

Easement





Title Plan - LT 581992

Created Parcels

Parcels

Area BA Deposited Plan 581992 Area BB Deposited Plan 581992 Area BC Deposited Plan 581992 Area BD Deposited Plan 581992 Area BE Deposited Plan 581992 Area BF Deposited Plan 581992

Total Area

Parcel Intent

Covenant - Land Easement Area RT Reference

2.5271 На

Schedule / Memorandum

Land Registration District			Survey Number
North Auckland		[LT 581992
Ferritorial Authority (the Council)			
Auckland Council			
		Schedule of Easemen	ts in Gross
		Last Edited: 03 Feb 202	3 07:56:02
Purpose	Shown	Burdened Land	Grantee
		(Servient Tenement)	
Right to drain water	В	Lot 7001	Auckland Council
	С	Lot 15	NZTA
	DA	Lot 16	NZTA
	DC	Lot 16	NZTA
	DB	Lot 16	NZTA
	EA	Lot 17	NZTA
	EB	Lot 17	NZTA
Right to convey telecommunications	Lot 6000	Lot 6000	Chorus New Zealand Limited
	Lot 6001	Lot 6001	Chorus New Zealand Limited
	Lot 6002	Lot 6002	Chorus New Zealand Limited
Right to convey electricity, gas	Lot 6000	Lot 6000	Vector Limited
	Lot 6002	Lot 6002	Vector Limited
	Lot 6001	Lot 6001	Vector Limited

Amalgamation Conditions

Last Edited: 30 Nov 2022 18:40:01

That Lot 6000 Hereon (legal access) be held as to ten undivided one-tenth shares by the owners of Lots 1 to 10 Hereon as tenants in common in the said shares and that individual Records of Title be issued in accordance therewith.

That Lot 6001 Hereon (legal access) be held as to six undivided one-sixth shares by the owners of Lots 24 to 29 Hereon as tenants in common in the said shares and that individual Records of Title be issued in accordance therewith.

That Lot 6002 Hereon (legal access) be held as to three undivided one-thrid shares by the owners of Lots 21 to 23 Hereon as tenants in common in the said shares and that individual Records of Title be issued in accordance therewith.

Schedule of Existing Easements to be Surrendered

Last Edited: 30 Nov 2022 18:41:01

Purpose	Shown	<u>Burdened Land</u> (Servient Tenement)	Creating Document Reference
Right of Way	Area A SO 503979	Section 15 SO 503979	T 5394299.1
Right to convey electricity	Area C SO 503979, Area E SO 503979, Area F SO 503979	Section 15 SO 503979	E 5331252.8

Covenants to be Revoked

Last Edited: 02 Dec 2022 08:42:59

Creating Document Reference GN 5331252.4

<u>Shown</u> Area B SO 503979, Area G SO 503979, Area L SO 503979, Area M SO 503979, Area D SO 503979

Page 1 of 2

Schedule / Memorandum

Land Registration District

Survey Number

Territorial Authority (the Council)

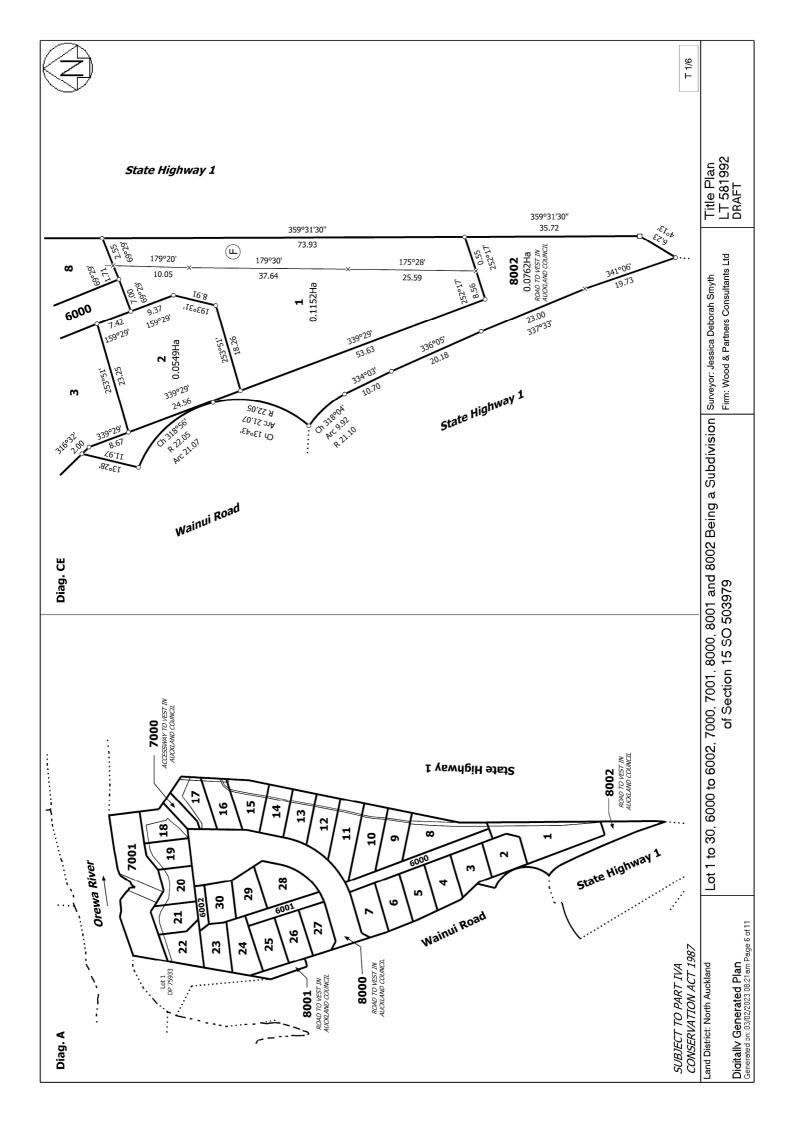
Notes

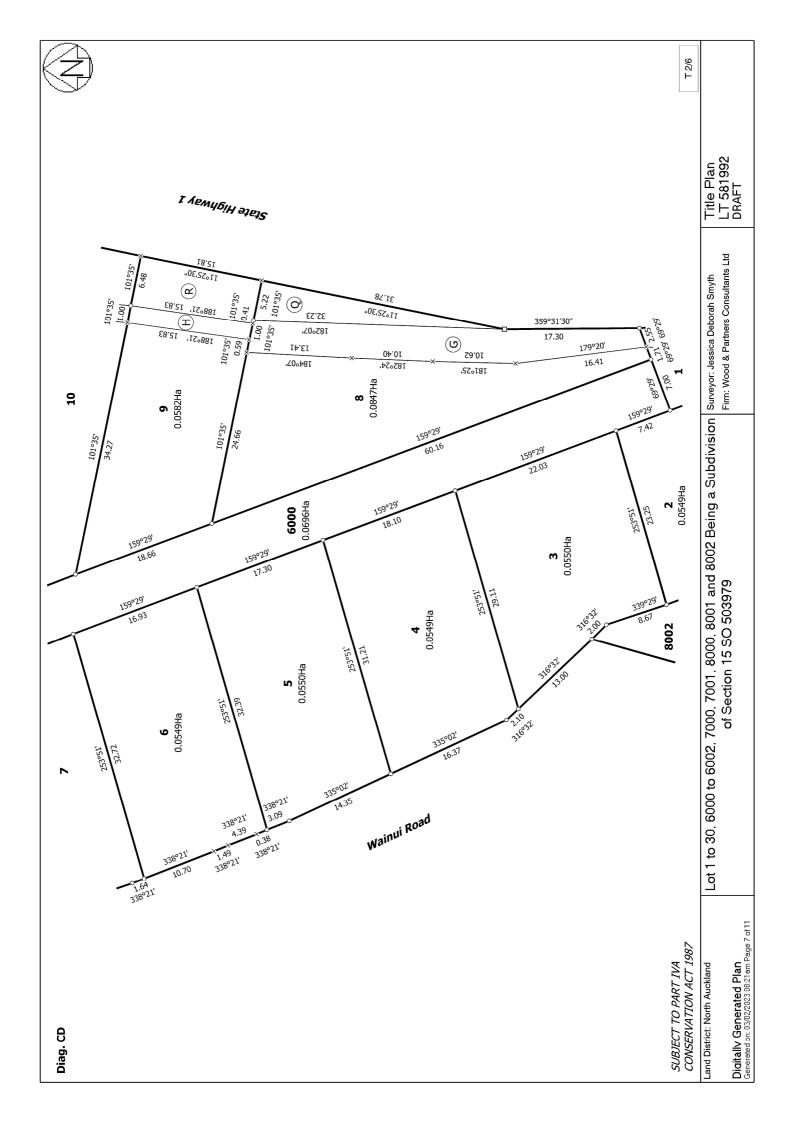
Last Edited: 03 Feb 2023 07:40:46

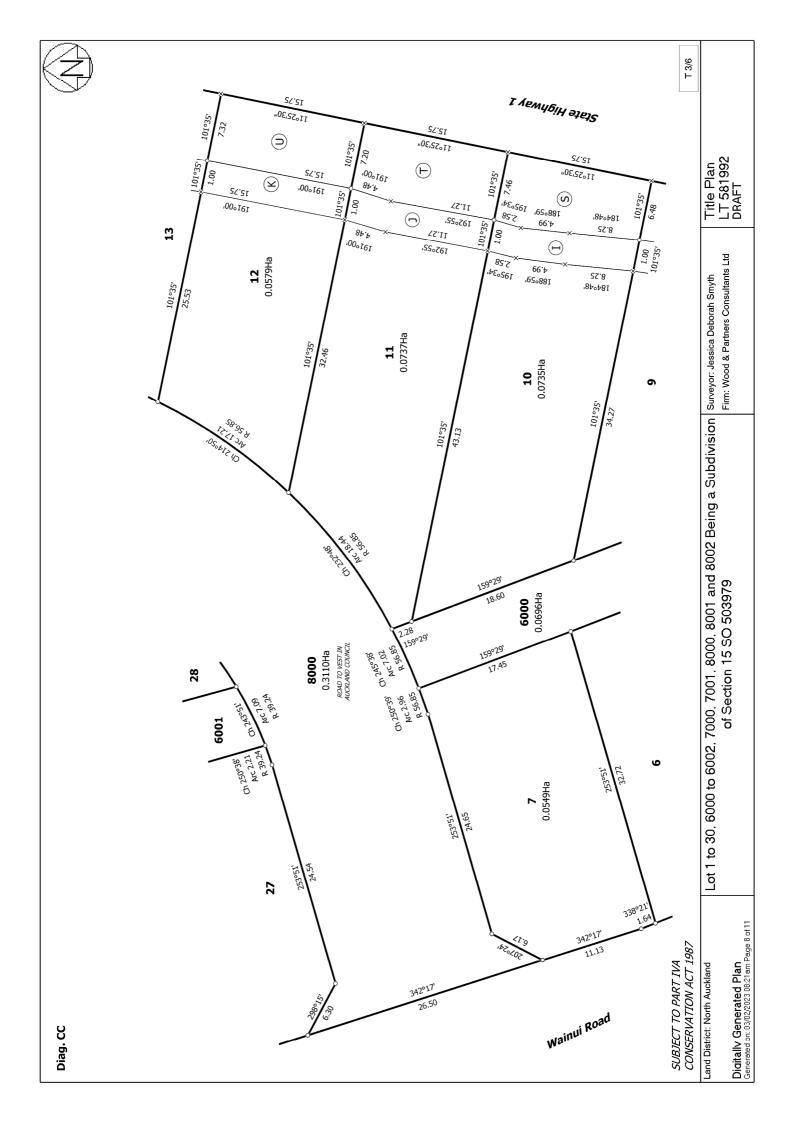
Areas BA to BF, DB, EB & F to O hereon are subject to land covenant - specific design area.

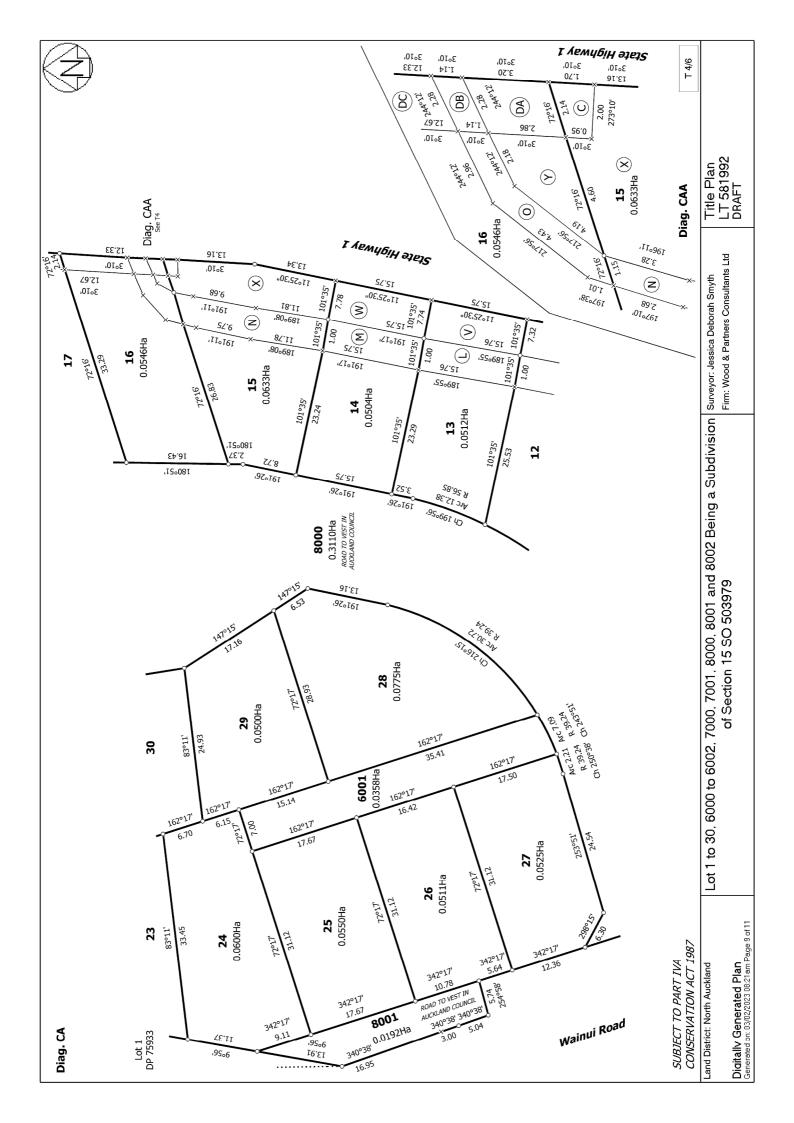
Areas Q to Y, DA & C hereon are subject to land covenant - no build zone.

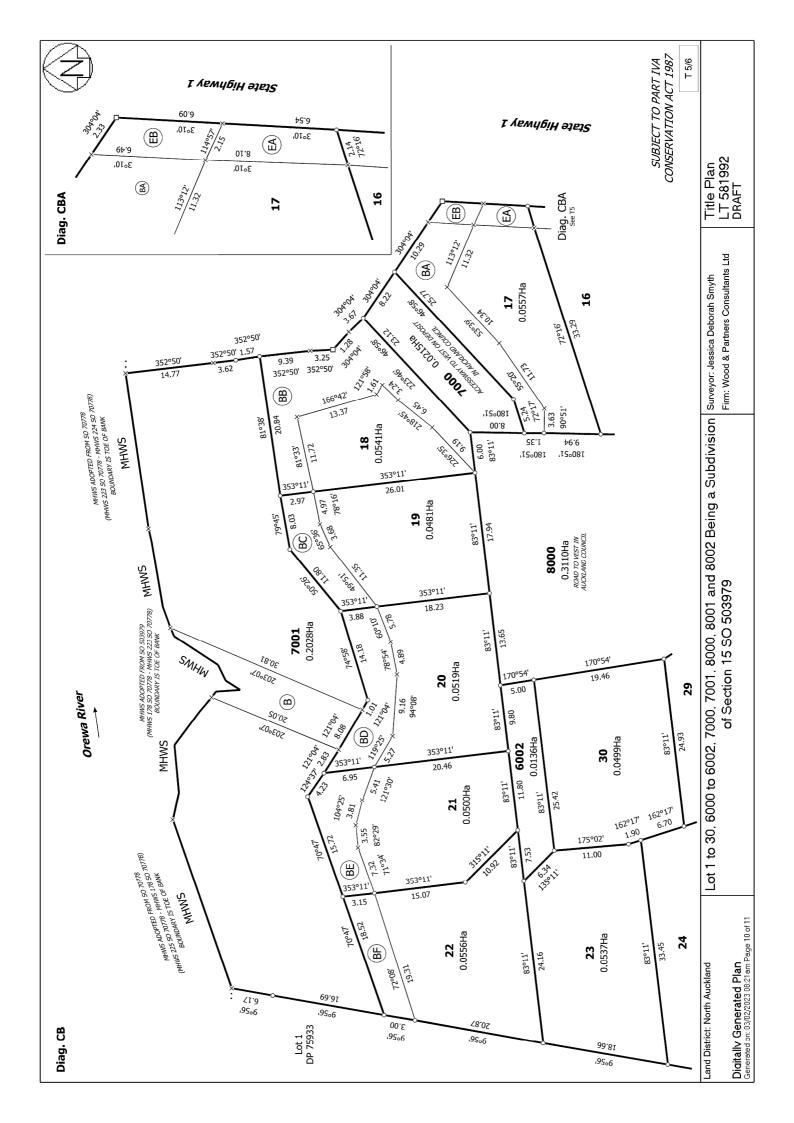
Page 2 of 2

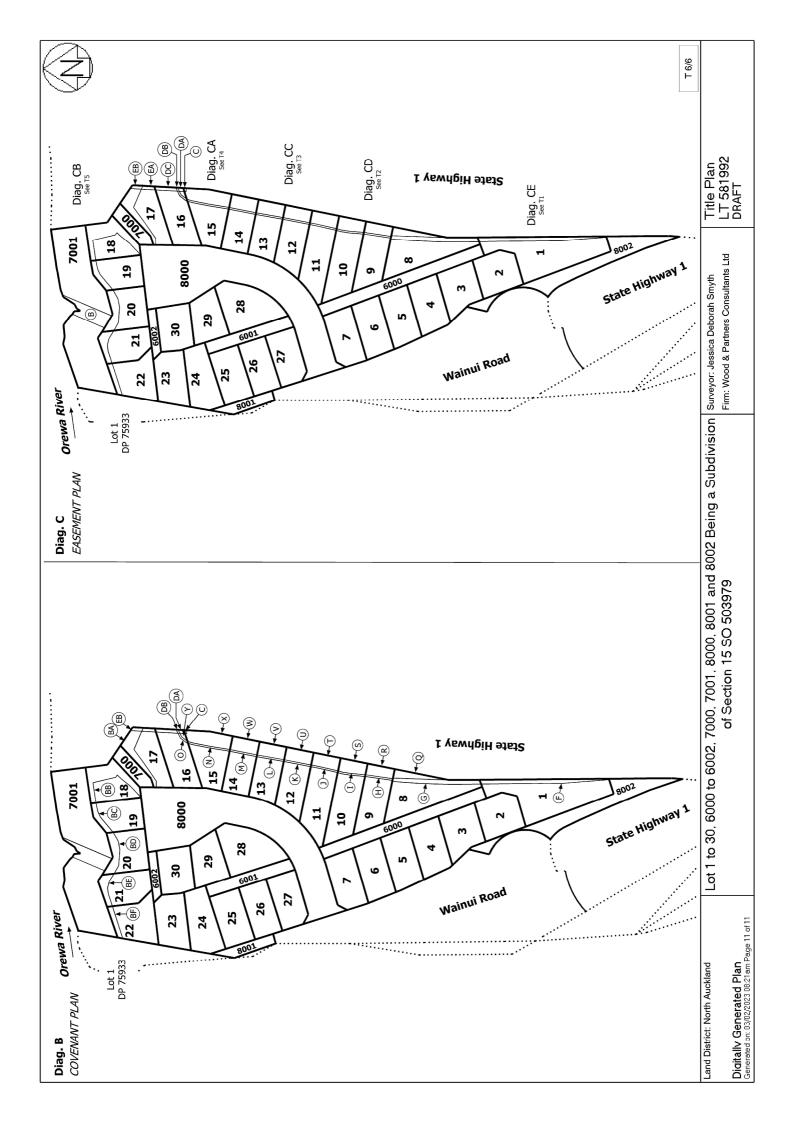


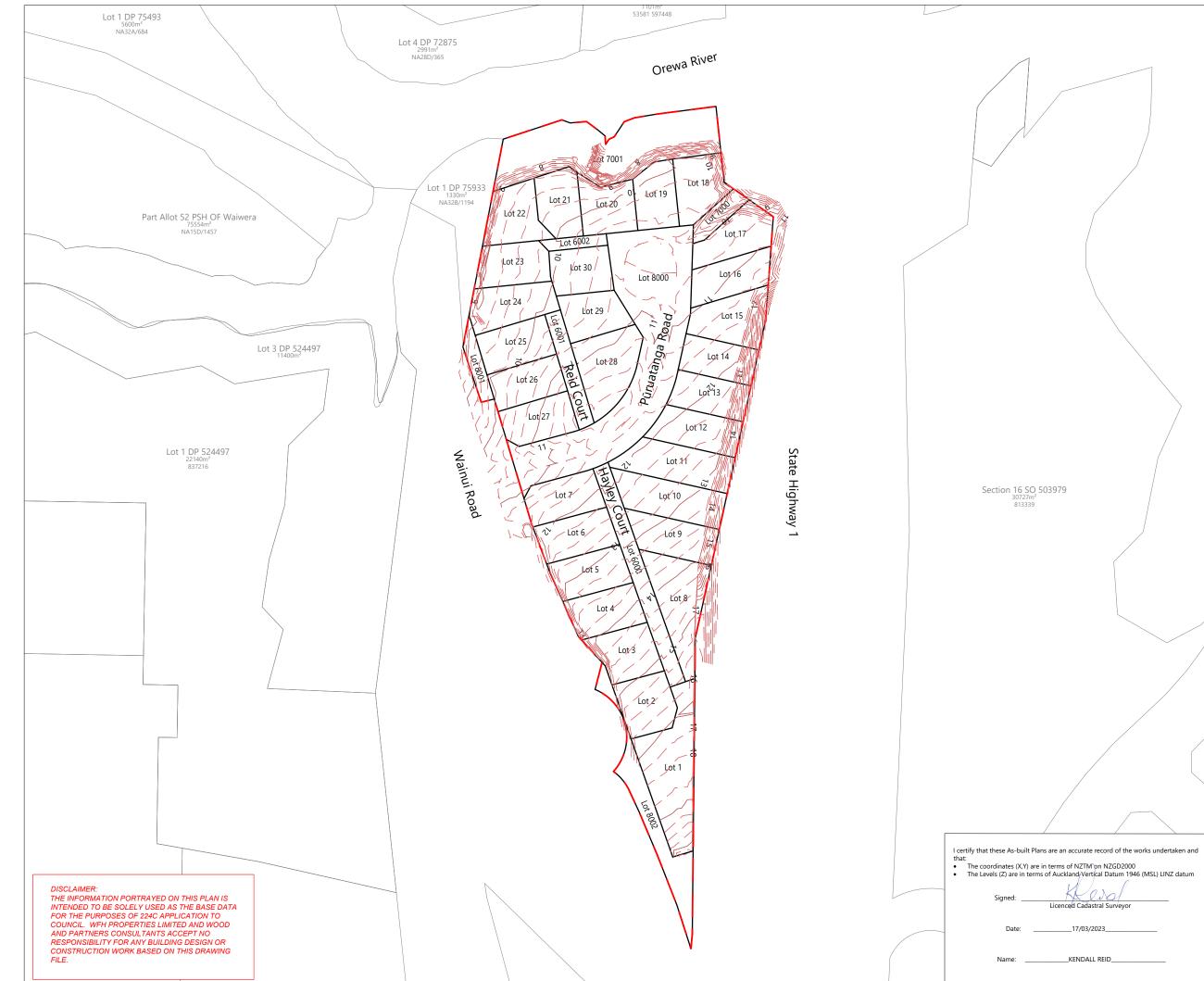














LEGEND:

MAJOR CONTOUR MINOR CONTOUR LOT BOUNDARIES STAGE BOUNDARY

NOTES:

_ _ _ _

- COORDINATES SHOWN ARE IN TERMS OF NEW ZEALAND
 TRANSVERSE MERCATOR (NZTM) PROJECTION
 LEVELS SHOWN ARE IN TERMS OF AUCKLAND VERTICAL DATUM
 1946
 CONTOURS ARE AT 0.25m INTERVALS
 BOUNDARIES ARE SUBJECT TO FINAL SURVEY AND LINZ
 APPROVAL

REVISION DETAILS		BY	DATE			
1	ISSUED FOR GCR			NN	13/12/22	
2	ISSUED FOR GCR FINAL		KR	14/03/23		
SU	RVEYED	WOODS	332 WAINUI ROAD			
DF	SIGNED	NC			UAD	

SURVETED	00003	332 WAINUI ROAD
DESIGNED	NC	WAINUI
DRAWN	EC	AUCKLAND
CHECKED	NC	
APPROVED	KR	WOODS.CO.NZ

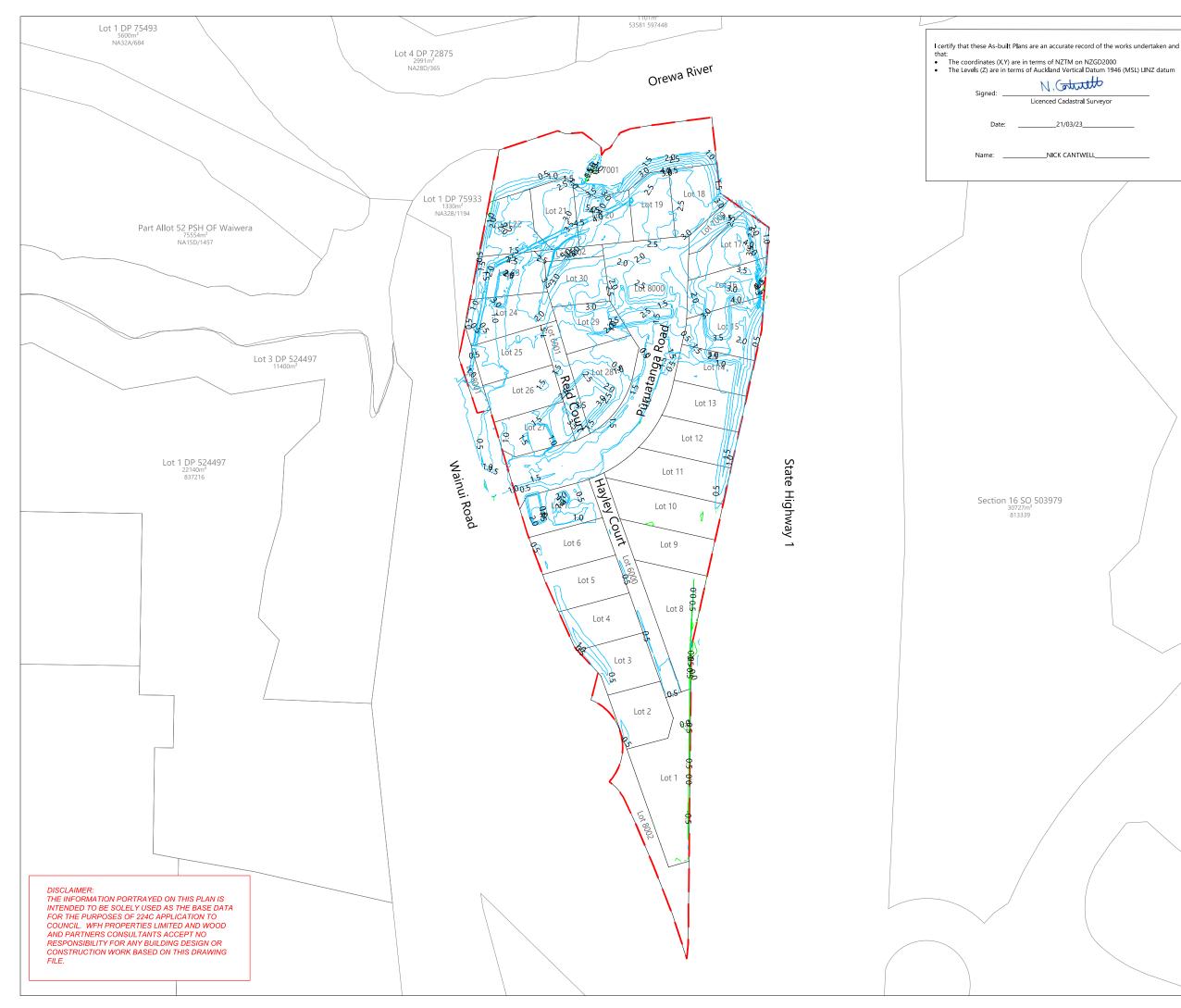


332 WAINUI ROAD

FINAL SURFACE ASBUILT OVERALL LAYOUT

STATUS	STATUS ISSUED FOR ASBUILT	
SCALE	1:1500 @ A3	
SCALE	1.1500 @ A3	2
COUNCIL	AUCKLAND COUNCIL	2
DWG NO	D10 276 00 1000 AD	
DWG NO P18-276-00-1000-AB		





STATUS	ISSUED FOR ASBUILT	REV
SCALE	1:1500 @ A3	2
COUNCIL	AUCKLAND COUNCIL	2
DWG NO P18-276-00-1111-AB		

CUT AND FILL ASBUILT

332 WAINUI ROAD

SHEET 2 OF 3

LOWEST TO FINAL SURFACE

 COORDINATES SHOWN ARE IN TERMS OF NEW ZEALAND
 TRANSVERSE MERCATOR (NZTM) PROJECTION
 LEVELS SHOWN ARE IN TERMS OF AUCKLAND VERTICAL DATUM
 1946 3. 4.

SURVEYED

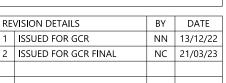
DESIGNED

DRAWN

CHECKED

APPROVED

N



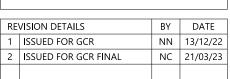
332 WAINUI ROAD

WAINU

AUCKLAND

WFH 🔶

WOODS.CO.NZ



1946 CONTOURS ARE AT 0.5m INTERVALS BOUNDARIES ARE SUBJECT TO FINAL SURVEY AND LINZ APPROVAL PLANS HAVE BEEN REVIEWED BY CMW GEOSCIENCE PLANS SHOULD BE READ IN CONJUNCTION WITH GCR

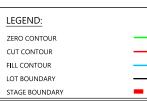
WOODS

CMW

EC

NC

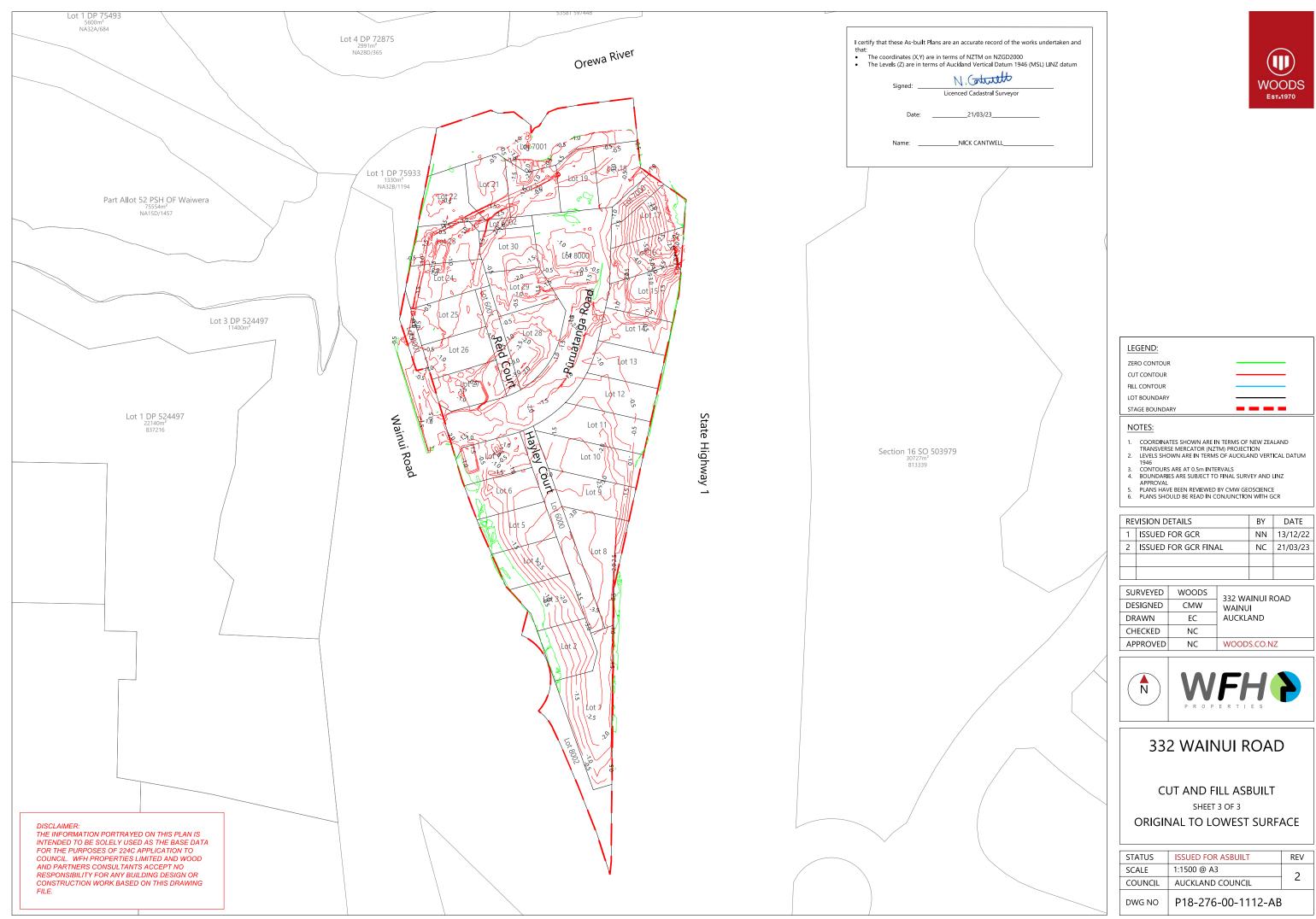
NC

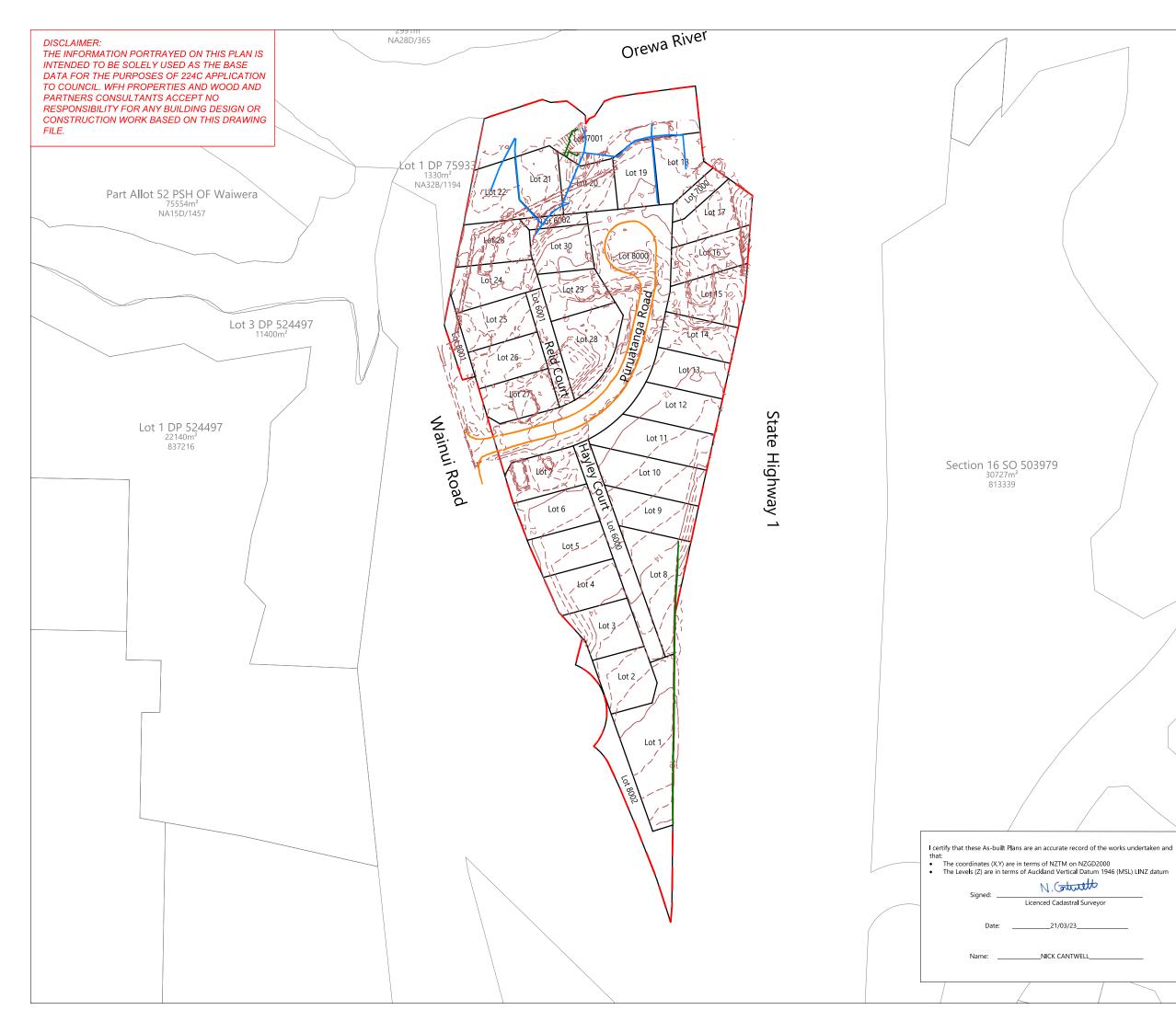


LEGEND:

NOTES:



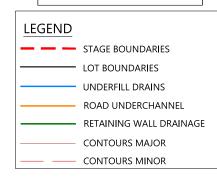






NOTES

- COORDINATES (X,Y) ARE IN TERMS OF NZTM ON NZGD2000
 LEVELS (Z) ARE IN TERMS OF AUCKLAND VERTICAL DATUM 1946 '(MSL) LINZ DATUM A LL DATA SUPPLIED BY CONTRACTOR
 CONTOURS ARE ARE OF LOWEST SURFACE AND AT 0.5m INTERVALS
 LOT BOUNDARIES SUBJECT TO FINAL SURVEY 6. SURVEY PLANS HAVE BEEN REVIEWED BY CMW GEOSCIENCE
 PLANS SHOULD BE READ IN CONJUCTION WITH GCR



REVISION DETAILS				BY	DATE
1	ISSUED FOR GCR FINAL		NC	21/03/23	
			1		
SU	RVEYED	WOODS	V	voods	Ltd
DESIGNED		NC	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFT		
DRAWN EC		EC	AUCKLAND 1023		1023
CHECKED NC		0	9 308 92	229	

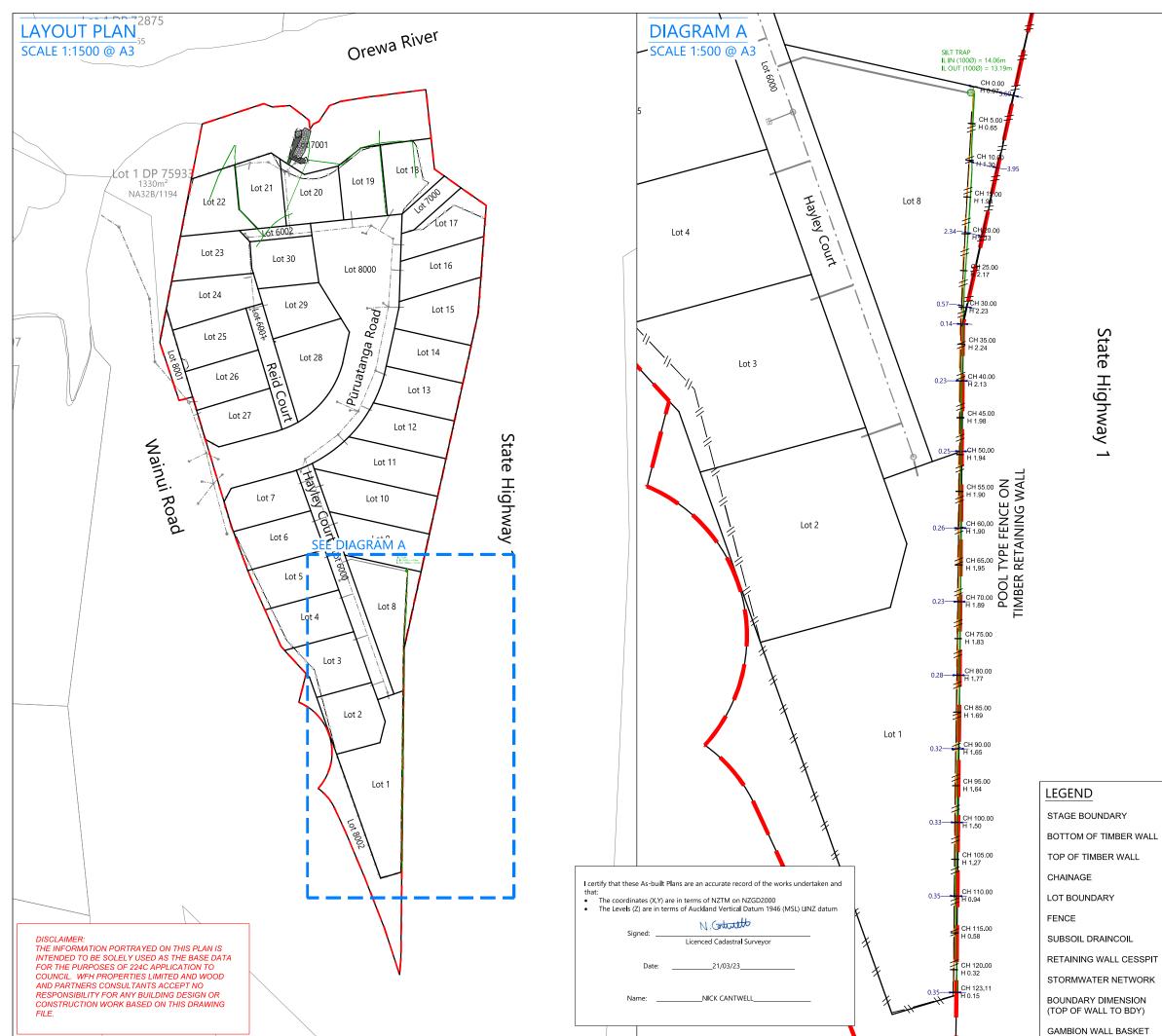
NC 09 308 9229 APPROVED KR WOODS.CO.NZ



332 WAINUI RD

SUBSOILS ASBUILT PLAN OVERALL LAYOUT

STATUS ISSUED FOR ASBUILT		REV
SCALE	1 : 1500 @ A3	1
COUNCIL	AUCKLAND COUNCIL	
DWG NO	P18-276-1200-AB	



TOP OF TIMBER WALL RETAINING WALL CESSPIT STORMWATER NETWORK

BOUNDARY DIMENSION (TOP OF WALL TO BDY)



NOTES

- . THIS PLAN HAS BEEN PREPARED IN ACCORDANCE WITH AUCKLAND COUNCIL BUILDING CONSENT REFERENCE BCO10342869.
- 2. COORDINATES ARE SHOWN IN TERMS OF NEW ZEALAND TRANSVERSE MERCATOR (NZTM) PROJECTION.
- 3. LEVELS SHOWN ARE IN TERMS OF AUCKLAND VERTICAL DATUM
- 4. ASBUILT DATA FOR ALL PRIVATE RETAINING WALL DRAINAGE HAS BEEN SUPPLIED BY THE CONTRACTOR.
- 5. UNLESS SHOWN OTHERWISE, ALL PRIVATE SUBSOIL DRAINAGE IS 110Ø POLYETHYLENE PERFORATED COLL DRAIN.
- UNLESS SHOWN OTHERWISE, ALL PRIVATE SW DRAINAGE IS 1000 uPVC SN16 PIPE.
- UNLESS SHOWN OTHERWISE, ALL PRIVATE & PUBLIC SILT TRAPS ARE 300mm x 300mm.

REVISION DETAILS					DATE
1	ISSUED FOR GCR			JS	13/12/22
2	ISSUED FOR GCR FINAL			KR	21/03/23
SURVEYED WOODS		332 WA			
DESIGNED NC				UAD	

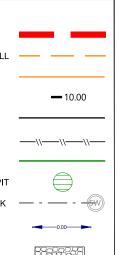
SURVEYED	WOODS	332 WAINUI ROAD
DESIGNED	NC	WAINUI
DRAWN	EC	AUCKLAND
CHECKED	NC	
APPROVED	NC	WOODS.CO.NZ

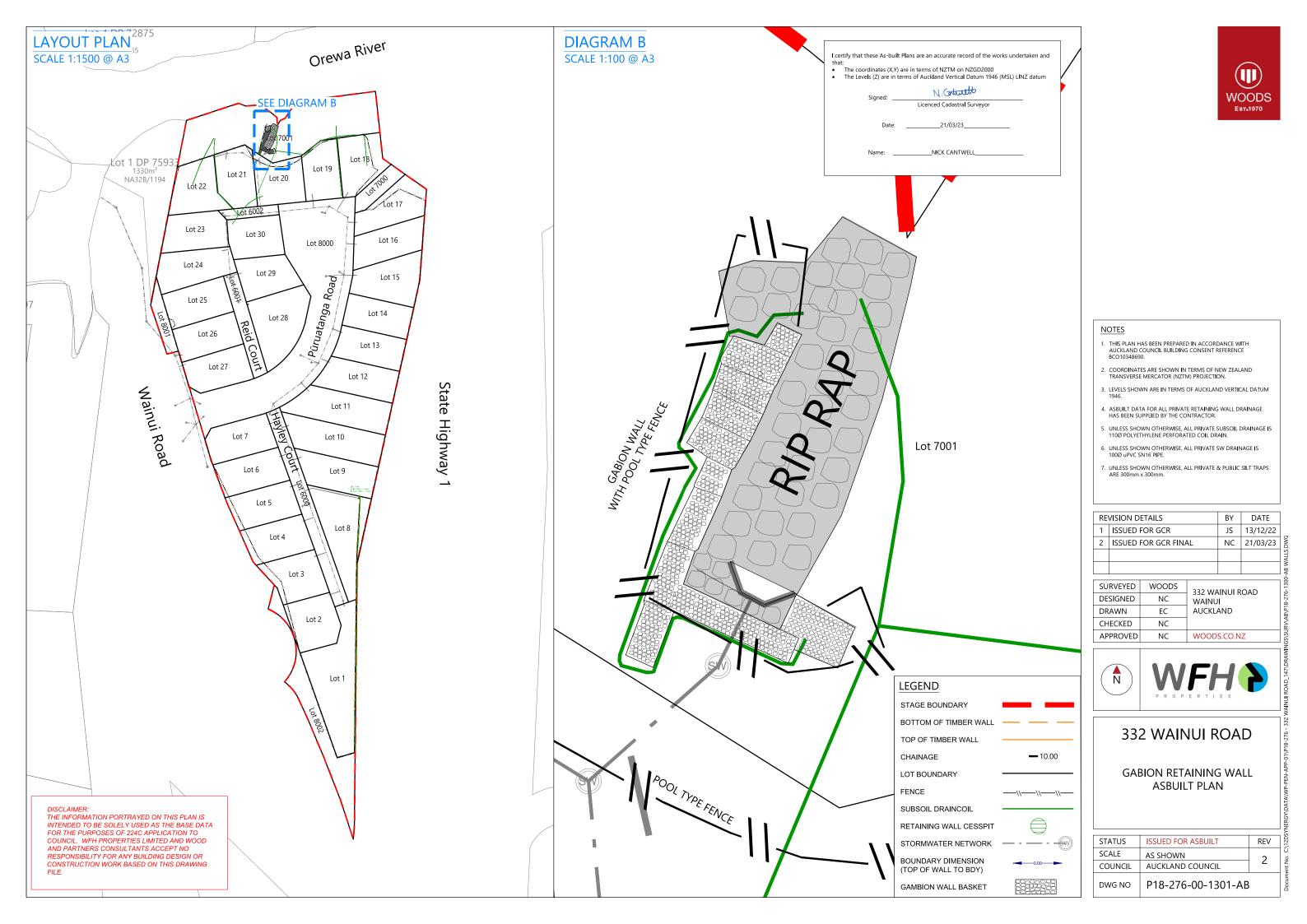


332 WAINUI ROAD

TIMBER RETAINING WALL ASBUILT PLAN

STATUS	ISSUED FOR ASBUILT	REV
SCALE	AS SHOWN	2
COUNCIL	AUCKLAND COUNCIL	2
DWG NO P18-276-00-1300-		









DISCLAIMER: THE INFORMATION PORTRAYED ON THIS PLAN IS INTENDED TO BE SOLELY USED AS THE BASE DATA FOR THE PURPOSES OF DISCUSSION. WFH PROPERTIES LTD AND WOOD AND PARTNERS CONSULTANTS ACCEPT NO RESPONSIBILITY FOR ANY BUILDING DESIGN OR CONSTRUCTION WORK BASED ON THIS DRAWING FILE.

LEGEND

LOT BOUNDARIES

UNDERLYING BOUNDARIES

REMEDIATED AREA





GAZETTE NOTICE 5394299.1 SUMMARY

The parts of the land within land marked B, M, D, L, and G on SO Plan 503979 are subject to the building restrictions contained in Gazette Notice 5331252.4 as imposed under Section 236 Public Works Act 1981.

REVISION DETAILS				BY	DATE
1	ISSUED	ISSUED FOR INFORMATION			24/02/23
511	RVEYED	WOODS			
30	RVETED	WOODS	WOODS Ltd		
DESIGNED				l 1 BUIL T STRFF	DING B T. GRAFTON
DRAWN		EC	AUCKLAND 1023		1023
CHECKED CM		CMW	09 308 9229		229

KR



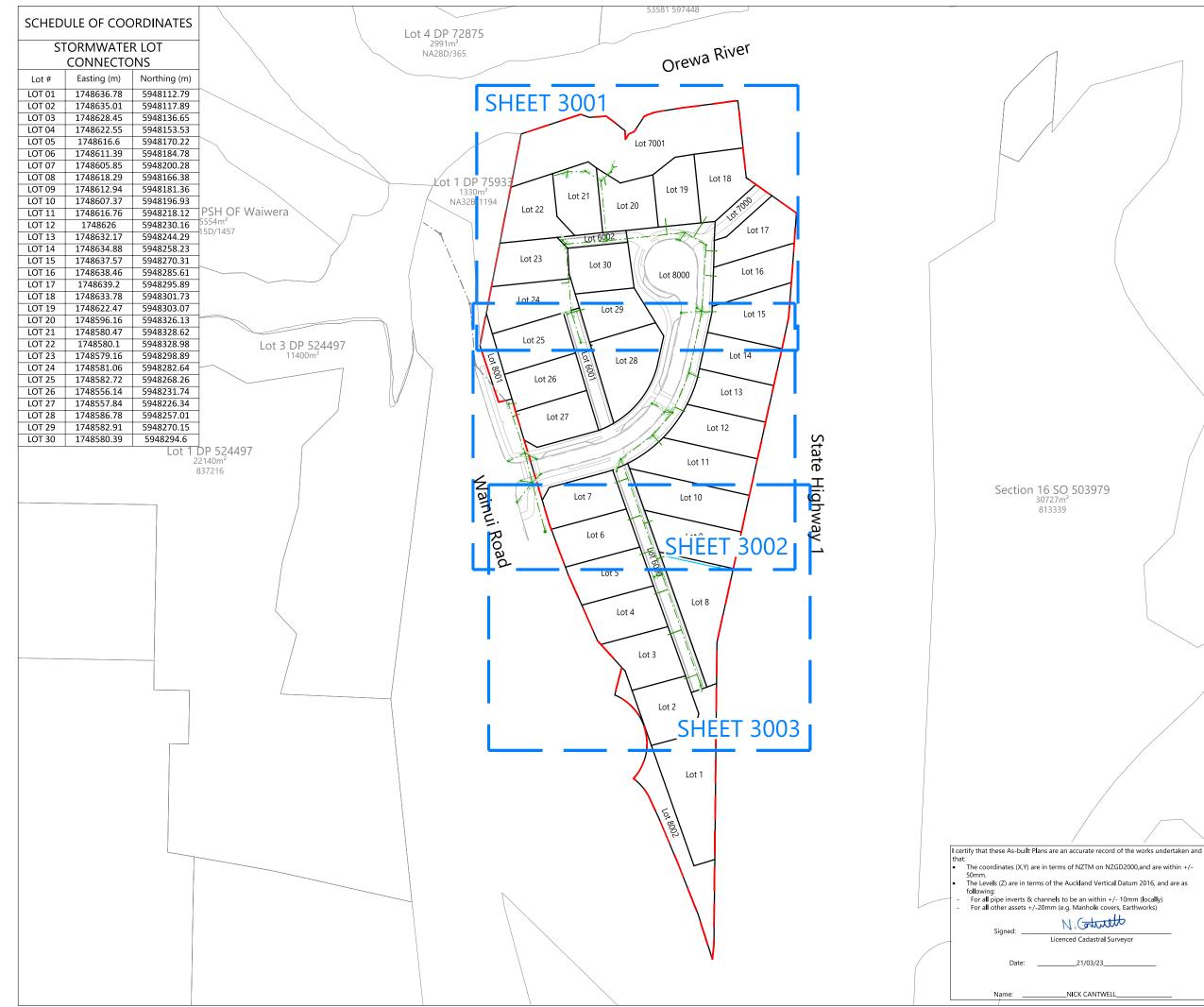


WOODS.CO.NZ

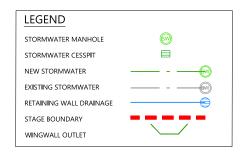
332 WAINUI RD

REMEDIATED AREAS

STATUS	AS-BUILT	REV
SCALE	1 : 1500 @ A3	1
COUNCIL	AUCKLAND COUNCIL	
DWG NO	P18-276-1400-AB	







NOTES

- 1. LOT CONNECTIONS ARE 100mm DIA uPVC.
- 2. ALL NEW MANHOLES ARE REINFORCED CONCRETE.
- 3. LOT BOUNDARIES ARE SUBJECT TO FINAL SURVEY AND LINZ APPROVAL
- 4. ASBUILT DATA HAS BEEN SOURCED FROM A COMBINATION OF WOODS SURVEY MEASURED DATA AND CONTRACTOR RECEIVED DATA.

REVISION DETAILS		BY	DATE	
1	ISSUED FOR INFORMATION	NC	21/03/23	

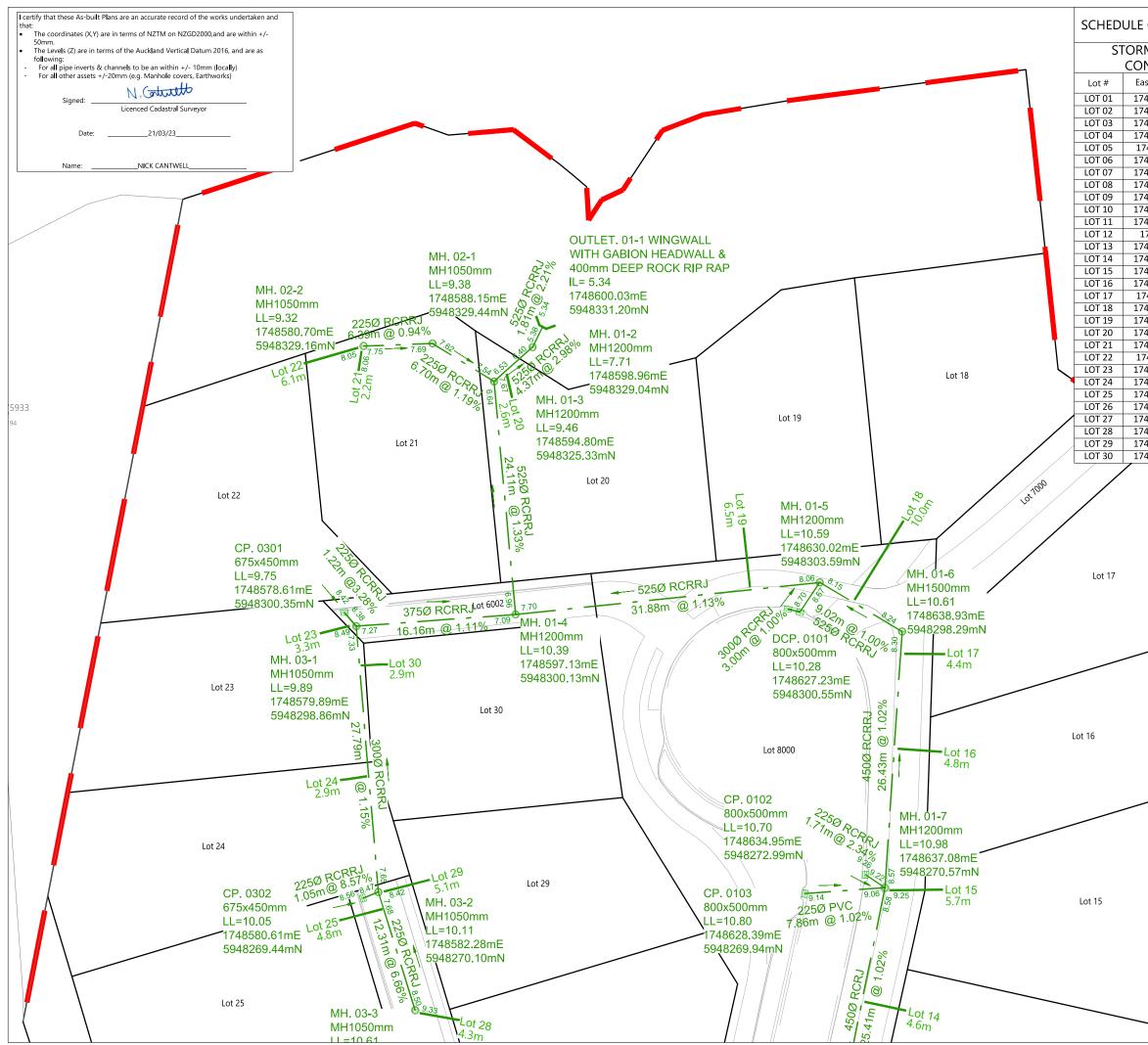
SURVEYED	WOODS	WOODS Ltd
DESIGNED	NC	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFTON
DRAWN	EC	AUCKLAND 1023
CHECKED	NC	09 308 9229
APPROVED	NC	WOODS.CO.NZ



332 WAINUI RD

STORMWATER ASBUILT OVERALL LAYOUT SHEET 1 OF 4

STATUS	AS-BUILT	REV
SCALE	1 : 1500 @ A3	1
COUNCIL	AUCKLAND COUNCIL	
DWG NO	P18-276-3000-AB	

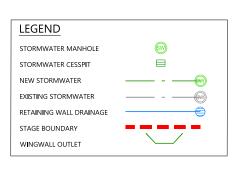


OF	COORDINATES

STORMWATER LOT

NNECTONS			
sting (m)	Northing (m)		
48636.78	5948112.79		
48635.01	5948117.89		
48628.45	5948136.65		
48622.55	5948153.53		
48616.6	5948170.22		
48611.39	5948184.78		
48605.85	5948200.28		
48618.29	5948166.38		
48612.94	5948181.36		
48607.37	5948196.93		
48616.76	5948218.12		
748626	5948230.16		
48632.17	5948244.29		
48634.88	5948258.23		
48637.57	5948270.31		
48638.46	5948285.61		
48639.2	5948295.89		
48633.78	5948301.73		
48622.47	5948303.07		
48596.16	5948326.13		
48580.47	5948328.62		
48580.1	5948328.98		
48579.16	5948298.89		
48581.06	5948282.64		
48582.72	5948268.26		
48556.14	5948231.74		
48557.84	5948226.34		
48586.78	5948257.01		
48582.91	5948270.15		
48580.39	5948294.6		





NOTES

- 1. LOT CONNECTIONS ARE 100mm DIA uPVC.
- 2. ALL NEW MANHOLES ARE REINFORCED CONCRETE.
- 3. LOT BOUNDARIES ARE SUBJECT TO FINAL SURVEY AND LINZ APPROVAL.
- 4. ASBUILT DATA HAS BEEN SOURCED FROM A COMBINATION OF WOODS SURVEY MEASURED DATA AND CONTRACTOR RECEIVED DATA.

REVISION DETAILS		BY	DATE		
1	ISSUED FOR INFORMATION		21/03/23		

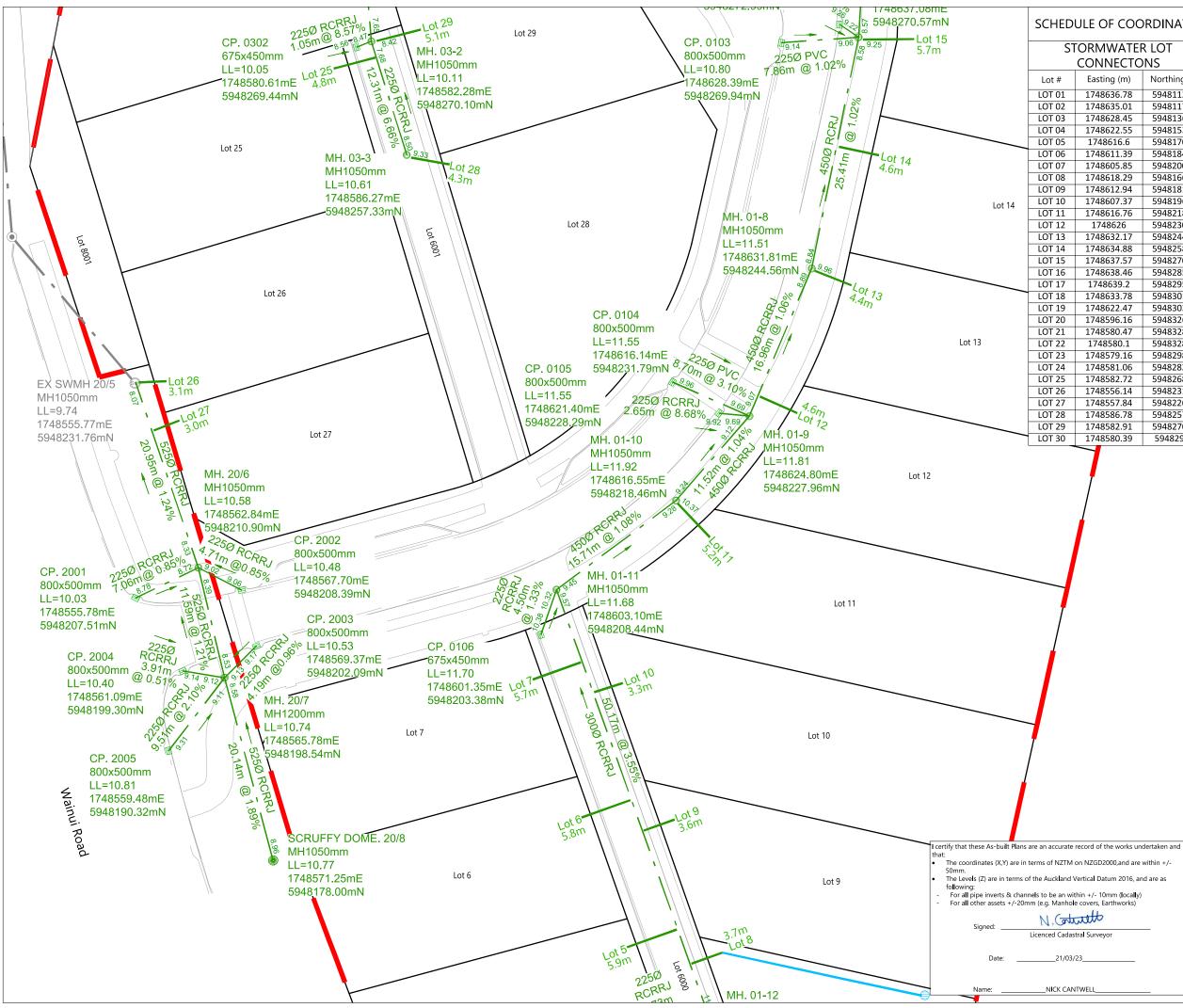
SURVEYED	WOODS	WOODS Ltd
DESIGNED	NC	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFTON
DRAWN	EC	AUCKLAND 1023
CHECKED	NC	09 308 9229
APPROVED	NC	WOODS.CO.NZ



332 WAINUI RD

STORMWATER ASBUILT SHEET 2 OF 4

STATUS	AS-BUILT	REV
SCALE	1 : 400 @ A3	1
COUNCIL	AUCKLAND COUNCIL	
DWG NO	P18-276-3001-AB	

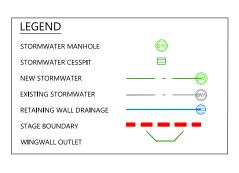


SCHEDULE OF COORDINATES

STORMWATER LOT CONNECTONS

NNECTONS				
sting (m)	Northing (m)			
48636.78	5948112.79			
48635.01	5948117.89			
48628.45	5948136.65			
48622.55	5948153.53			
48616.6	5948170.22			
48611.39	5948184.78			
48605.85	5948200.28			
48618.29	5948166.38			
48612.94	5948181.36			
48607.37	5948196.93			
48616.76	5948218.12			
748626	5948230.16			
48632.17	5948244.29			
48634.88	5948258.23			
48637.57	5948270.31			
48638.46	5948285.61			
48639.2	5948295.89			
48633.78	5948301.73			
48622.47	5948303.07			
48596.16	5948326.13			
48580.47	5948328.62			
48580.1	5948328.98			
48579.16	5948298.89			
48581.06	5948282.64			
48582.72	5948268.26			
48556.14	5948231.74			
48557.84	5948226.34			
48586.78	5948257.01			
48582.91	5948270.15			
48580.39	5948294.6			





NOTES

- 1. LOT CONNECTIONS ARE 100mm DIA uPVC.
- 2. ALL NEW MANHOLES ARE REINFORCED CONCRETE.
- 3. LOT BOUNDARIES ARE SUBJECT TO FINAL SURVEY AND LINZ APPROVAL
- 4. ASBUILT DATA HAS BEEN SOURCED FROM A COMBINATION OF WOODS SURVEY MEASURED DATA AND CONTRACTOR RECEIVED DATA.

REVISION DETAILS			BY	DATE
ISSUED FOR INFORMATION		NC	21/03/23	
		ISSUED FOR INFORM	ISSUED FOR INFORMATION	ISSUED FOR INFORMATION NC

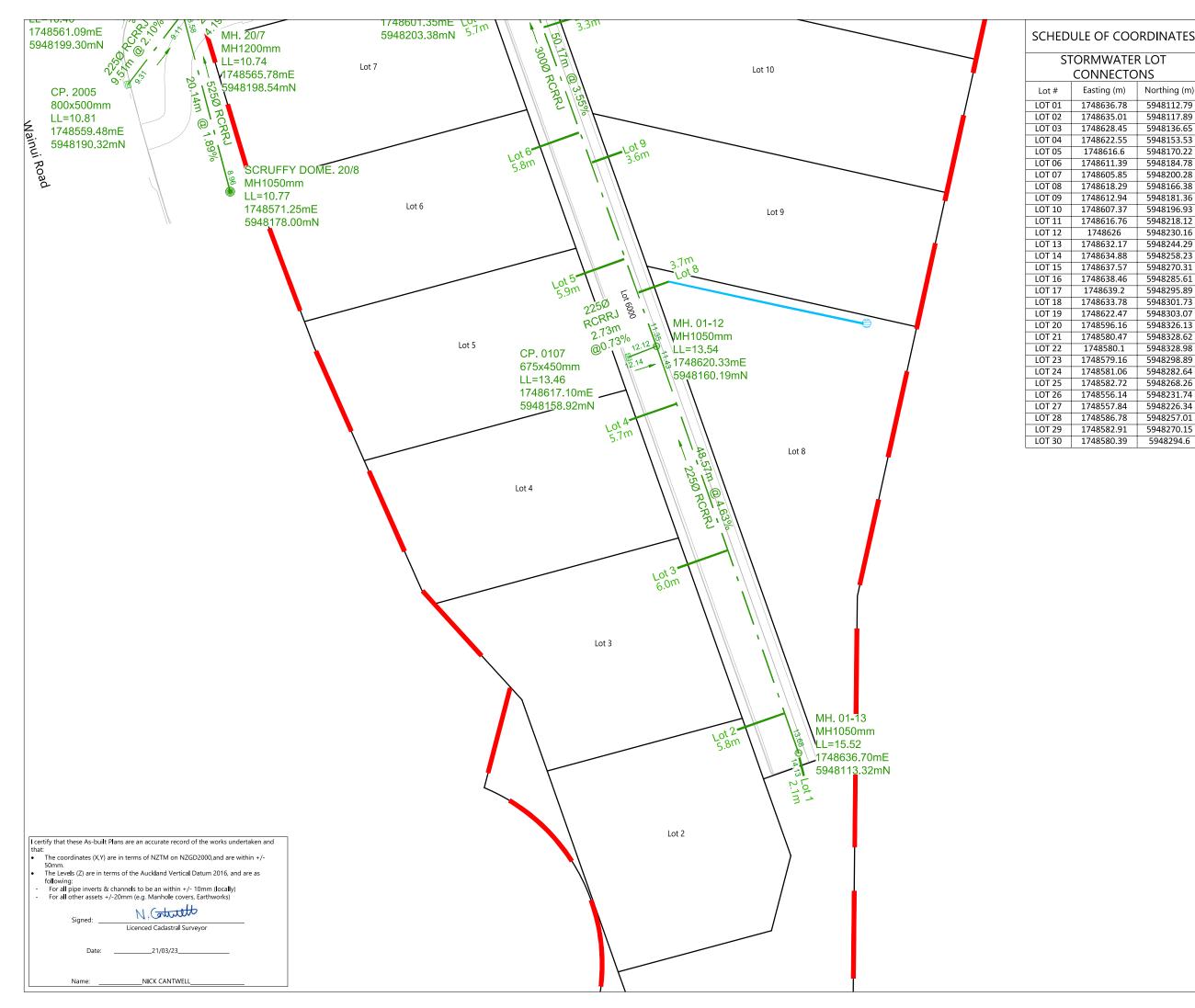
SURVEYED	WOODS	WOODS Ltd
DESIGNED	NC	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFTON
DRAWN	EC	AUCKLAND 1023
CHECKED	NC	09 308 9229
APPROVED	NC	WOODS.CO.NZ



332 WAINUI RD

STORMWATER ASBUILT SHEET 3 OF 4

STATUS	AS-BUILT	REV
SCALE	1 : 400 @ A3	1
COUNCIL	AUCKLAND COUNCIL	
DWG NO	P18-276-3002-AB	

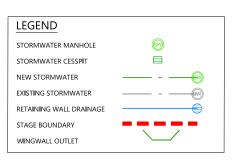


SCHEDULE OF COORDINATES

TORMWATER LOT	
CONNECTONS	

NINECTOINS					
sting (m)	Northing (m)				
48636.78	5948112.79				
48635.01	5948117.89				
48628.45	5948136.65				
48622.55	5948153.53				
48616.6	5948170.22				
48611.39	5948184.78				
48605.85	5948200.28				
48618.29	5948166.38				
48612.94	5948181.36				
48607.37	5948196.93				
48616.76	5948218.12				
748626	5948230.16				
48632.17	5948244.29				
48634.88	5948258.23				
48637.57	5948270.31				
48638.46	5948285.61				
48639.2	5948295.89				
48633.78	5948301.73				
48622.47	5948303.07				
48596.16	5948326.13				
48580.47	5948328.62				
48580.1	5948328.98				
48579.16	5948298.89				
48581.06	5948282.64				
48582.72	5948268.26				
48556.14	5948231.74				
48557.84	5948226.34				
48586.78	5948257.01				
48582.91	5948270.15				
48580.39	5948294.6				





NOTES

- 1. LOT CONNECTIONS ARE 100mm DIA uPVC.
- 2. ALL NEW MANHOLES ARE REINFORCED CONCRETE.
- 3. LOT BOUNDARIES ARE SUBJECT TO FINAL SURVEY AND LINZ APPROVAL.
- 4. ASBUILT DATA HAS BEEN SOURCED FROM A COMBINATION OF WOODS SURVEY MEASURED DATA AND CONTRACTOR RECEIVED DATA.

REVISION DETAILS			BY	DATE	
1	ISSUED FOR INFORMATION		NC	21/03/23	
SURVEYED WOODS				VOODS	144

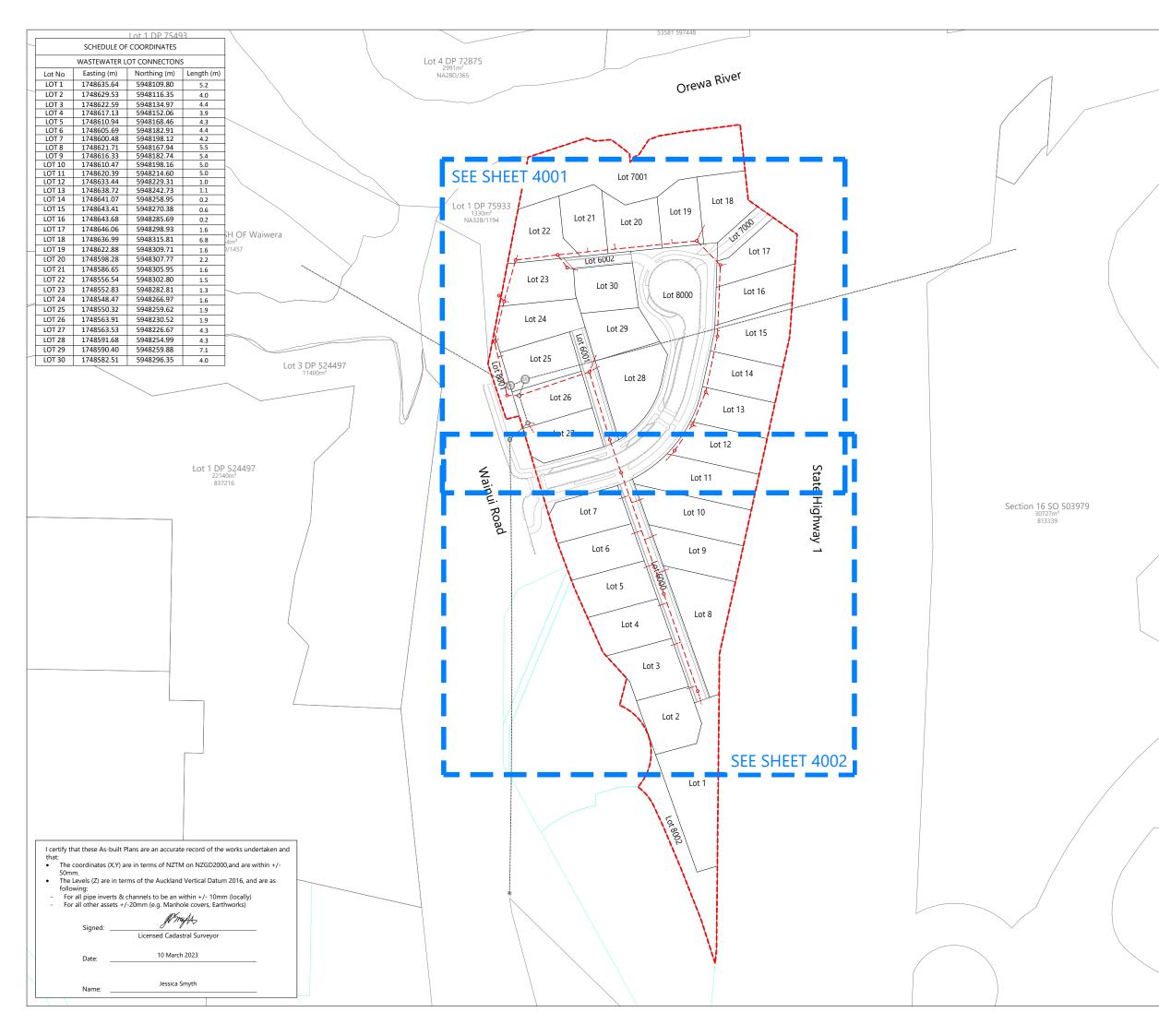
JORVETED	100005	WOODS Ltd
DESIGNED	NC	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFTON
DRAWN	EC	AUCKLAND 1023
CHECKED	NC	09 308 9229
APPROVED	NC	WOODS.CO.NZ



332 WAINUI RD

STORMWATER ASBUILT SHEET 4 OF 4

STATUS	AS-BUILT	REV
SCALE	1 : 400 @ A3	1
COUNCIL	AUCKLAND COUNCIL	
DWG NO	P18-276-3003-AB	





DISCLAIMER:

DISCLAIMER: THE INFORMATION PORTRAYED ON THIS PLAN IS INTENDED TO BE SOLELY USED AS THE BASE DATA FOR THE PURPOSES OF 224C APPLICATION TO COUNCIL. WTH PORPERTIES AND WOOD AND PARTNERS CONSULTANTS ACCEPT NO RESPONSIBILITY FOR ANY BUILDING DESIGN OR CONSTRUCTION WORK BASED ON THIS DRAWING FILE.

LEGEND

NEW SANITARY SEWER MANHOLE NEW SANITARY SEWER EXISTING SANITARY SEWER MANHOLE

EXISTING SANITARY SEWER

LOT BOUNDARIES

STAGE BOUNDARY

<u>(55)</u>

S

NOTES

- 1. LOT BOUNDARIES ARE SUBJECT TO FINAL SURVEY.
- 2. ALL PIPE AND MH DIAMETERS ARE INTERNAL, AND SHOWN IN MILLIMETERS UNLESS OTHERWISE SPECIFIED.
- 3. LOT CONNECTIONS ARE TWO-DIMENSIONAL LENGTHS.
- 4. PIPE LENGTHS ARE THREE-DIMENSIONAL LENGTHS TO ALLOW FOR THE PRACTICAL EFFECT OF THE GRADE.
- 5. ASBUILT DATA HAS BEEN SOURCED FROM A COMBINATION OF WOODS SURVEY MEASURED DATA AND CONTRACTOR RECEIVED DATA.

RE	VISION DETAILS	BY	DATE
1	ISSUED FOR INFORMATION	EC	10/03/23

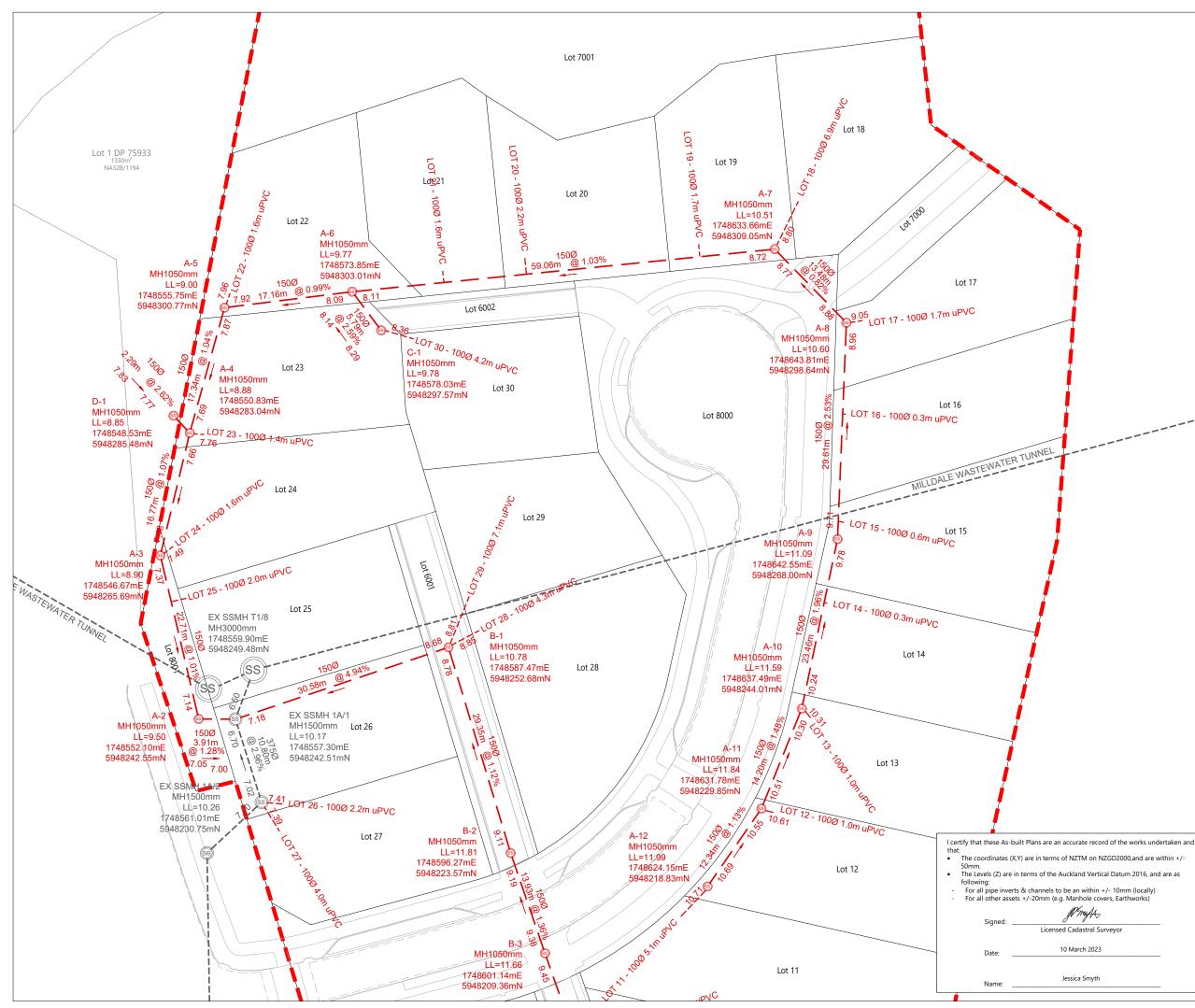
WOODS	WOODS Ltd
WOODS	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFTON
EC	AUCKLAND 1023
JS	09 308 9229
JS	WOODS.CO.NZ
	WOODS EC JS



332 WAINUI RD

WASTEWATER ASBUILT OVERALL LAYOUT SHEET 1 OF 3

STATUS	ISSUED FOR INFORMATION	REV		
SCALE	1:1500 @ A3	1		
COUNCIL	AUCKLAND COUNCIL	I		
DWG NO	P18-276-00-4000-AB			





S

SS

DISCLAIMER: THE INFORMATION PORTRAYED ON THIS PLAN IS INTENDED TO BE SOLLY USED AS THE BASE DATA FOR THE PURPOSES OF 224C APPLICATION TO COUNCIL. WFH PORPERTIES AND WOOD AND PARTNERS CONSULTANTS ACCEPT NO RESPONSIBILITY FOR ANY BUILDING DESIGN OR CONSTRUCTION WORK BASED ON THIS DRAWING FILE.

LEGEND

NEW SANITARY SEWER MANHOLE NEW SANITARY SEWER

EXISTING SANITARY SEWER MANHOLE

EXISTING SANITARY SEWER

LOT BOUNDARIES

STAGE BOUNDARY

NOTES

- LOT BOUNDARIES ARE SUBJECT TO FINAL SURVEY.
- ALL PIPE AND MH DIAMETERS ARE INTERNAL, AND 2. SHOWN IN MILLIMETERS UNLESS OTHERWISE SPECIFIED.
- 3. LOT CONNECTIONS ARE TWO-DIMENSIONAL LENGTHS.
- 4. PIPE LENGTHS ARE THREE-DIMENSIONAL LENGTHS TO ALLOW FOR THE PRACTICAL EFFECT OF THE GRADE.
- ASBUILT DATA HAS BEEN SOURCED FROM A 5. COMBINATION OF WOODS SURVEY MEASURED DATA AND CONTRACTOR RECEIVED DATA.

RE	VISION DETAILS	BY	DATE
1	ISSUED FOR INFORMATION	EC	10/03/23

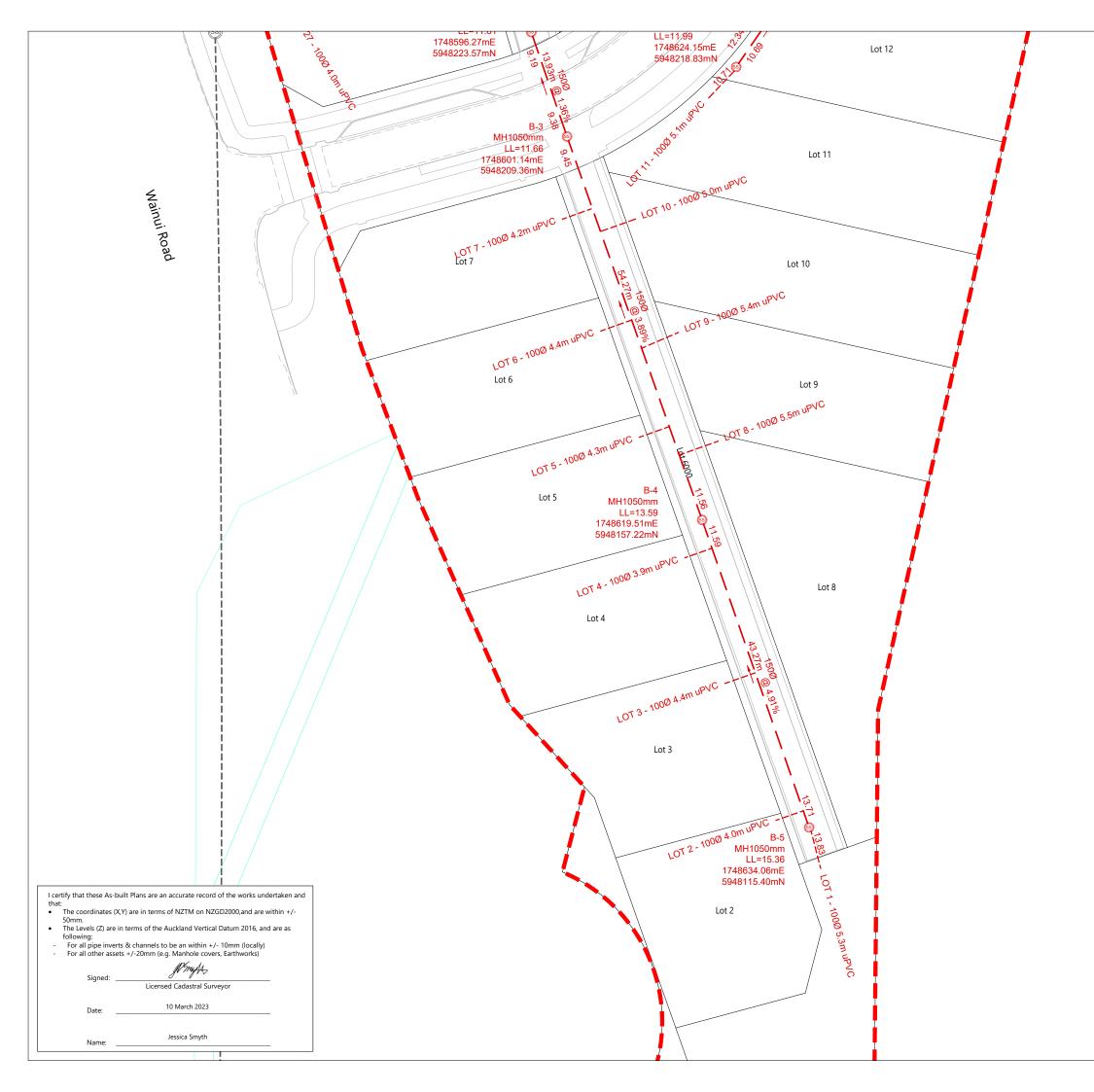
SURVEYED	WOODS	WOODS Ltd
DESIGNED	WOODS	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFTON
DRAWN	EC	AUCKLAND 1023
CHECKED	JS	09 308 9229
APPROVED	JS	WOODS.CO.NZ



332 WAINUI RD

WASTEWATER ASBUILT SHEET 2 OF 3

STATUS	ISSUED FOR INFORMATION	REV
SCALE	1:500 @ A3	1
COUNCIL	AUCKLAND COUNCIL	I
DWG NO	P18-276-00-4001-AB	





S

SS

DISCLAIMER: THE INFORMATION PORTRAYED ON THIS PLAN IS INTENDED TO BE SOLELY USED AS THE BASE DATA FOR THE PURPOSES OF 224C APPLICATION TO COUNCIL. WHY PROPERTIES AND WOOD AND PARTNERS CONSULTANTS ACCEPT NO RESPONSIBILITY FOR ANY BUILDING DESIGN OR CONSTRUCTION WORK BASED ON THIS DRAWING FILE.

LEGEND

NEW SANITARY SEWER MANHOLE NEW SANITARY SEWER

EXISTING SANITARY SEWER MANHOLE

EXISTING SANITARY SEWER

LOT BOUNDARIES

STAGE BOUNDARY

NOTES

- 1. LOT BOUNDARIES ARE SUBJECT TO FINAL SURVEY.
- 2. ALL PIPE AND MH DIAMETERS ARE INTERNAL, AND SHOWN IN MILLIMETERS UNLESS OTHERWISE SPECIFIED.
- 3. LOT CONNECTIONS ARE TWO-DIMENSIONAL LENGTHS.
- 4. PIPE LENGTHS ARE THREE-DIMENSIONAL LENGTHS TO ALLOW FOR THE PRACTICAL EFFECT OF THE GRADE.
- ASBUILT DATA HAS BEEN SOURCED FROM A 5. COMBINATION OF WOODS SURVEY MEASURED DATA AND CONTRACTOR RECEIVED DATA.

RE	VISION DETAILS	BY	DATE
1	ISSUED FOR INFORMATION	EC	10/03/23
			-,, -

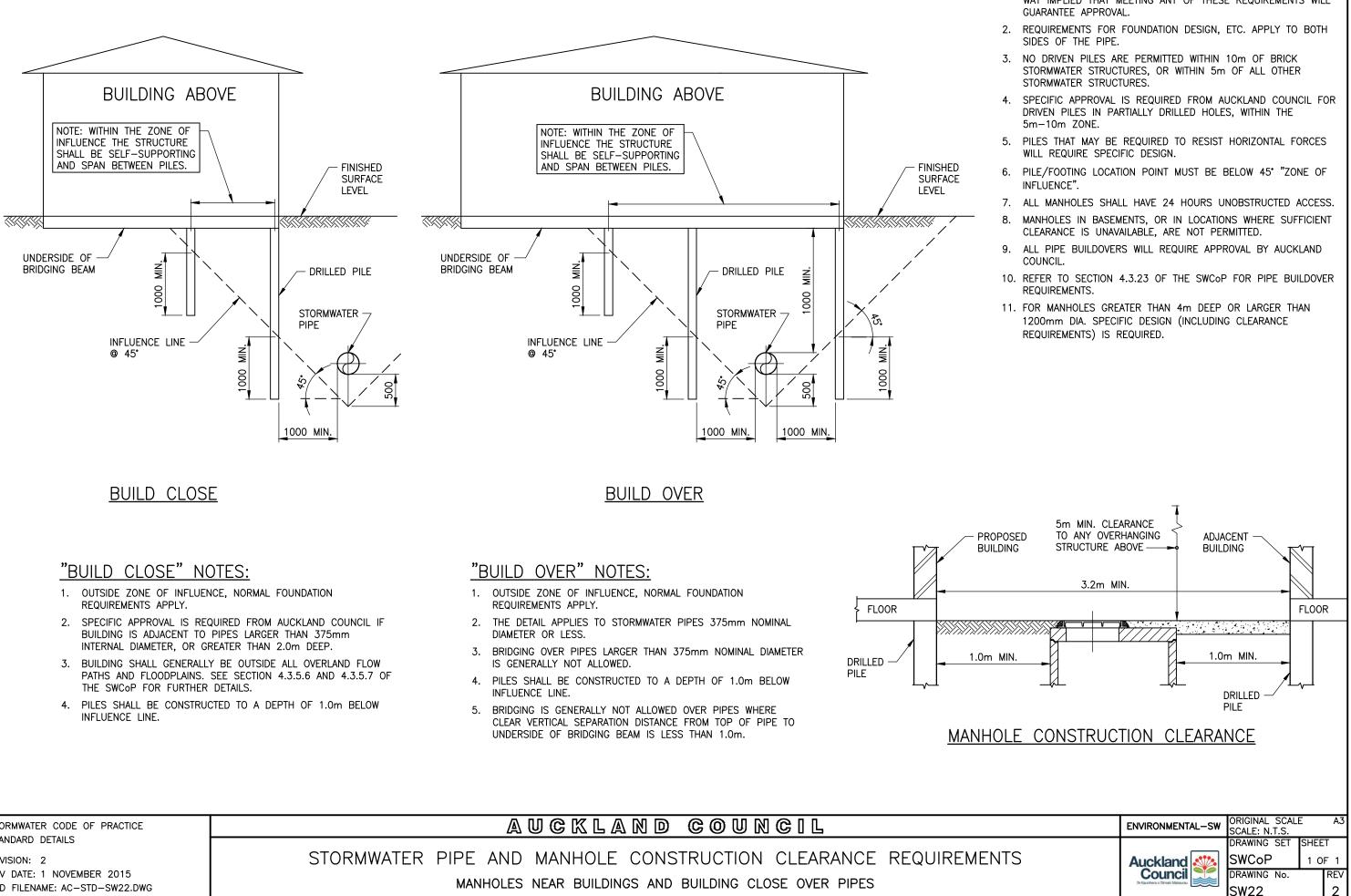
SURVEYED	WOODS	WOODS Ltd
DESIGNED	WOODS	LEVEL 1 BUILDING B 8 NUGENT STREET, GRAFTON
DRAWN	EC	AUCKLAND 1023
CHECKED	JS	09 308 9229
APPROVED	JS	WOODS.CO.NZ
		1



332 WAINUI RD

WASTEWATER ASBUILT SHEET 3 OF 3

STATUS	ISSUED FOR INFORMATION	RFV
SCALE	1:500 @ A3	
COUNCIL	AUCKLAND COUNCIL	1
DWG NO	P18-276-00-4002-AB	



STORMWATER CODE OF PRACTICE STANDARD DETAILS

N

REVISION: 2 REV DATE: 1 NOVEMBER 2015 CAD FILENAME: AC-STD-SW22.DWG

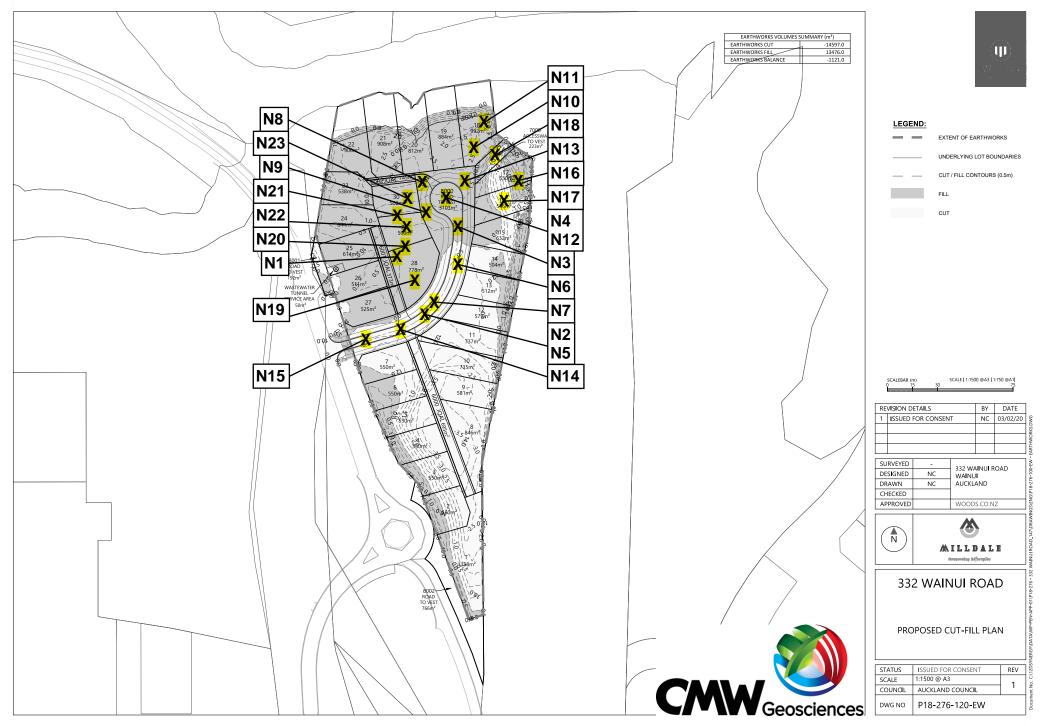
GENERAL NOTES:

- 1. THE INFORMATION ON THIS PAGE IS INTENDED TO SHOW EXAMPLES OF TYPICAL SCENARIOS AND SHALL BE USED FOR GENERAL GUIDANCE PURPOSES ONLY. SIGNIFICANT VARIATIONS ON A SITE-BY-SITE BASIS ARE TO BE EXPECTED AND IT IS IN NO WAY IMPLIED THAT MEETING ANY OF THESE REQUIREMENTS WILL

Appendix D: Field Test Data

CM	WGeosci	LF11 Rev.15 Soil Fiel	d Density NDM Dir	ect Tran	smissi	on wi	th VS	S Rep	ort (C	Cohes	ive So	oils)		11/63, Arrenv	hnical NZ Limi way Drive, Ros 06, Albany, Aud	edale, NZ 0632				
Project:		332 Wainui Road												Test Metho	ds:	Notes:	Solid Densit	y:		Assumed
Project No:		AKL2019-0182															Solid Densit	y Data Sourc	e:	N/A
Location:		Wainui Road												NZS 4407 20)15 Test 3.1 🔇	,	Testing Loca	tions Selecte	ed By:	CMW Field Staff
Report No:		AKL2019-0182LAA Rev.1												NZS 4407 20)15 Test 4.2		♦ Only samp	les <2.0mm	will be consid	ered for endorsed
Report Date:		22/12/2022												NZGS:Augus	st 2001		testing			
Client:		Fulton Hogan Land Development Limited												-			(1) Blade size	e of 19mm use	ed.	
Client Address	:	PO Box 501, Silverdale, 0944													FRANK LABORA	accredite	s indicated as not d are outside the he laboratory's		Measuremen	ts marked * are not accredited e the scope of the laboratories accreditation
					Vane	e ID	Ir	i-situ Va	ne Shear	Strength	s			Fie	eld and Labora	tory Testing I	Data			
Date Sampled	Sample No.	Test Location*	Soil Description*	Solid Density (t/m³) *	Head #	Blade #	Test 1 (kPa)	Test 2 (kPa)	Test 3 (kPa)	Test 4 (kPa)	Ave.	Gauge Wet Density (t/m³) **	Gauge Dry Density (t/m ³)	Gauge Water Content (%)	Gauge Air Voids (%)	Gauge Probe Depth (mm)	Oven Water Content (%)	Oven Dry Density (t/m ³)	Oven Calculated Air Voids (%) *	Comments
18/01/2021	N1	Refer to site plan	Blended ROCK/CLAY	2.70	2327	2327	181	206	215	215	204	1.90	1.44	32.4	0	300	24.8	1.52	2 6	
	N2	Refer to site plan	Blended ROCK/CLAY	2.70	2327	2327	147	181	UTP	UTP	164+	1.75	1.44	21.2	16	300	19.0	1.47	18	
	N3	Refer to site plan	Blended ROCK/CLAY	2.70	2327	2327	95	74	114	104	97	1.58	0.98	61.4	4	300	44.4	1.09	11	
19/01/2022	N4	Culvert backfill	Blended CLAY/ROCK	2.70	2327	2327	141	215	169	199	181	1.71	1.20	42.1	5	300	40.7	1.21	6	
	N5	СН68	Blended CLAY/ROCK	2.70	2327	2327	138	135	215	141	157	1.93	1.46	31.7	C	300	33.5	1.44	4 -2	Retest of N2
20/01/2022	N6	Roadbox CH99	Blended CLAY/ROCK	2.70	2327	2327	215	144	138	160	164	1.91	1.44	32.4	C	300	29.6	1.47	2	
	N7	Roadbox CH77	Blended CLAY/ROCK	2.70	2327	2327	215	215	172	184	197	1.98	1.58	25.3	1	300	21.1	1.64	s	
25/01/2022	N8	Roadbox turnstile	Blended CLAY/ROCK	2.70	2327	2327	215	215	135	184	187	1.74	1.21	44.3	2	300	34.5	1.30	7	
	N9	Roadbox turnstile	Blended CLAY/ROCK	2.70	2327	2327	187	172	163	141	166	1.75	1.12	56.2	-5	300	34.3	1.30	7	
1/02/2022	N10	Refer to site plan	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.97	1.52	29.8	-1	300	27.3	1.54	1	
	N11	Refer to site plan	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	169	204	1.93	1.48	30.6	C	300	27.1	1.52	2 2	
3/02/2022	N12	Refer to site plan	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.79	1.36	32.2	6	300	29.1	1.39	8	
	N13	Refer to site plan	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.80	1.40	28.8	8	300	22.2	1.47	13	
14/02/2022	N14	Roadbox backfill	Blended CLAY/ROCK	2.70	2327	2327	169	215	215	203	201	1.77	1.34	31.7	8	300	28.5	1.37	10	
	N15	Roadbox backfill	Blended CLAY/ROCK	2.70	2327	2327	147	190	175	181	173	1.89	1.28	47.7	-8	300	27.7	1.48	8 4	
28/02/2022	N16	Lot 17	Blended CLAY/ROCK	2.70	2327	2327	138	156	172	181	162	1.71	1.21	41.3	5	300	36.3	1.26	8	
	N17	Lot 17	Blended CLAY/ROCK	2.70	2327	2327	169	187	163	150	167	1.83	1.39	31.2	5	300	38.1	1.32	2 1	
	N18	Lot 17	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.97	1.56	26.0	1	300	25.2	1.57	2	
11/03/2022	N19	Lot 28	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.88	1.47	28.1	4	300	22.7	1.54	8	
	N20	Lot 28	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.84	1.41	30.0	5	300	22.8	1.49	11	
	N21	Lot 27	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.91	1.53	25.1	5	300	22.5	1.56	5 7	
16/03/2022	N22	Lot 29	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.89	1.47	28.6	3	300	22.8	1.54	۱ 8	
	N23	Lot 30	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.87	1.42	32.2	2	300	21.0	1.55	5 10	
15/03/2022	N24	* No data or site plan for this point																		
	N25	* No data or site plan for this point																		
	N26	* No data or site plan for this point																		
This report ch	ould only h	e reproduced in full.										** Gauge Wet	Densities outsid	e of the calibrate	ed range of 1.75	4 to 2.611 t/m ³	are not accredite	d and are outsi	de the laboratori	es scope of accreditation.
		reports numbered AKL2019-0182LAA	Rev.0									3								
Created By:		AMS	Date:	25/01/	2022															
Checked By:		RS	Date:	22/12/																
	gnatory:	JLM	Date:	22/12/																Page: 1 of 2

AKL2019-0182LAA Rev. 1



Geosciences

LF14 Rev.13 Dynamic Cone Penetration (DCP) Test Report

CMWGeos	sciences		Li 14 Nevi 13			5 4402: 1988 Test	6.5.2	,				
Project:		Milldale 332 Wainu	ui Road									
Project No:		AKL2019-0182				Auckland Labor CMW Geoscien	ratory ices (NZ) Ltd Partnership					
Location:		Wainui Road					ay Drive, Rosedal , Albany, Aucklar					
Report No:		AKL2019-0182LAB	Rev.0			Phone: +64 (09						
Test Date:		17/03/2022				Testing Locatio	ns Selected By:		CMW Field Staf	f		
		SDM					ns selected by.			•		
Tested By:						CCRED.	1760					
Client:		Fulton Hogan Land	Development Limit	ed			Test results in accredited of scope of the	idicated as not are outside the laboratory's	accredited and are	R Values are not outside the scope of		
Client Address:		15 Sir William Picke	ering Drive, Burnside	e, Christchurch 8053	8	STING LAS	accreditatio	n	the laboratory	's accreditation		
CBR Test Calculation:		Austroad (2010)										
Test No		1		2		3		4				
Test Location	Ro	ad 1	Roa	ad 1	Ro	ad 1	Roa	ad 1				
Chainage & Offset	Cł	124	CH	140	CI	460	CH	180				
Material & Layer			SG/Pr	e Stabilised CLA	Y 330mm below	surface		-				
Depth (mm)	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*		
0 - 100	17	20+	12	20+	13	20+	13	20+				
100 - 200	6	13	5	10	8	18	15	20+				
200 - 300	4	8	4	8	8	18	7	15				
300 - 400	2	4	3	6	5	10	15	20+				
400 - 500	1	2	6	13	7	15	10	20+				
500 - 600	3	6	6	13	7	15	8	18				
600 - 700	1	2	6	13	16	20+	12	20+				
700 - 800	3	6	9	20	10	20+	10	20+				
800 - 900	2	4	10	20+			8	18				
900 - 1000	3	6	13	20+			8	18				
Test No												
Test Location												
Chainage & Offset												
Material & Layer												
Depth	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*		
0 - 100												
100 - 200												
200 - 300												
300 - 400												
400 - 500												
500 - 600												
600 - 700												
700 - 800	ļ											
800 - 900												
900 - 1000							ļ					
Created by:	JLM			Date:	17/03/2022		This report should only be reproduced in full *Equivalent CBR values calculated using AUSTROADS (2010) Guide to Pavement Technology Part 2, Figure 5.3, For Fine Grained Cohesive Soils, and					
Checked by:	RS			Date:	26/07/2022		are	relevant to fine gra	ined cohesive soils o	nıy.		
Authorised Signatory:	JLM			Date:	27/07/2022		Page 1 of 2					

Milldale 332 Wainui Road



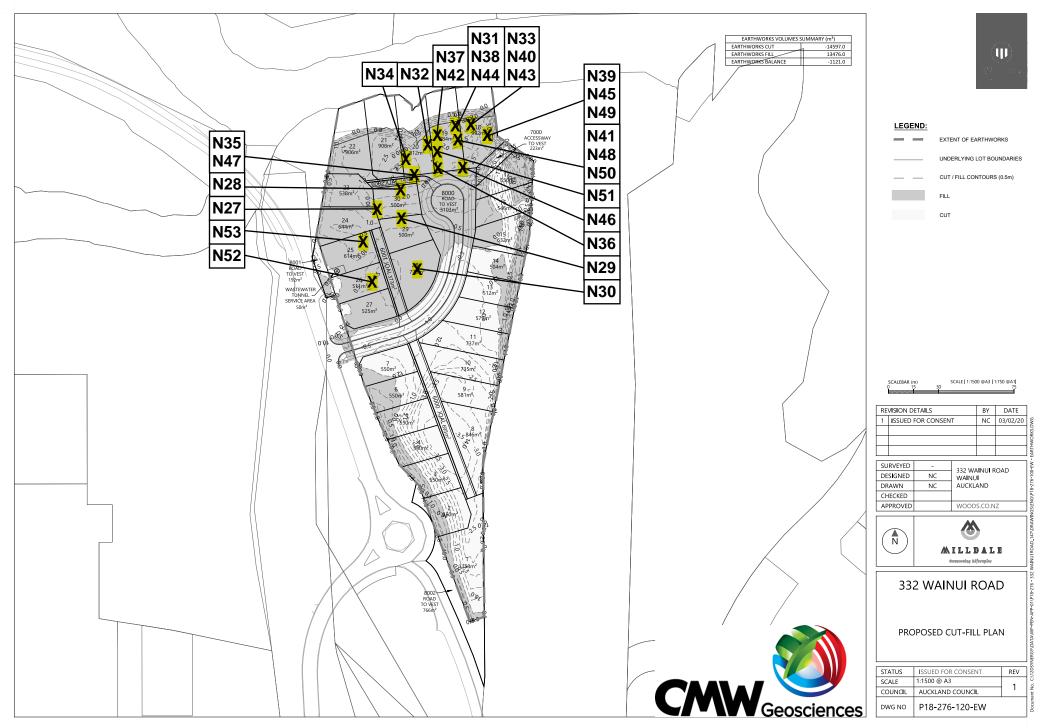


CMI	N Geosci	LF11 Rev.15	s Soil Field	Density NDM [Direct Trai	nsmiss	sion w	vith V	SS Re	eport (Cohe	sive S	ioils)		11/63, Arrenv	ences (NZ) Ltd vay Drive, Ros 16, Albany, Aud	Partnership edale, NZ 0632 ckland, NZ 0752					
Project:		Milldale 332 Wainui Road													Test Metho	ds:	Notes:	Solid Densit	y:		Assumed	
Project No:		AKL2019-0182																Solid Densit	y Data Sourc	e:	N/A	
Location:		Wainui Road													NZS 4407 20	15 Test 3.1 (٥	Testing Loca	ations Selecte	ed By:	CMW Fiel	d Staff
Report No:		AKL2019-0182LAC Rev.0													NZS 4407 20	15 Test 4.2		♦ Only samp	oles <2.0mm	will be consid	ered for er	ndorsed
Report Date:		26/07/2022													NZGS:Augus	t 2001		testing				
Client:		Fulton Hogan Land Developmer	nt Limited															1) Blade size	e of 19mm use	d.		
Client Address:		15 Sir William Pickering Drive, B	urnside, Christchu	ırch 8053												FRING LABORA	Test result accredite scope of t	s indicated as not d are outside the he laboratory's tion				re not accredited f the laboratories n
		Test Location*	k			Van	e ID	h	n-situ Va	ne Shear	Strength	s			Fi	eld and Labor	atory Testing [Data				
Date Sampled S	ample No.	Test Area	RL/Details	Soil Description*	Solid Density (t/m ³) *	Head #	Blade #	Test 1 (kPa)	Test 2 (kPa)	Test 3 (kPa)	Test 4 (kPa)	Ave.	Gauge Wet Density (t/m ³) **	Gauge Dry Density (t/m ³)	Gauge Water Content (%)	Gauge Air Voids (%)	Gauge Probe Depth (mm)	e Oven Water Content (%)	Oven Dry Density (t/m ³)	Oven Calculated Air Voids (%) *	Co	mments
30/03/2022 N	127	Lot 30	-	Blended CLAY/ROCK	2.70	2327	2327	199	156	215	117	172	1.81	1.33	35.8	3	3 300	25.3	1.45	10		
N	128	Lot 30	-	Blended CLAY/ROCK	2.70	2327	2327	172	215	172	190	187	1.88	1.43	31.3	2	2 300	35.9	1.38	-1		
N	129	Lot 29	-	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.92	1.48	29.5	1	1 300	23.3	1.56	6		
N	130	Lot 28	-	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.91	1.52	25.6	5	5 300	24.4	1.53	6		
4/04/2022 N	131	Shear Key Undercut	-	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	206	213	1.85	1.44	28.9	5	5 300	28.9	1.43	5		
N	132	Shear Key Undercut	-	Blended CLAY/ROCK	2.70	2327	2327	141	147	199	153	160	1.81	1.38	31.7	5	5 300	26.8	1.43	9		
N	133	General Fill Area	-	Blended CLAY/ROCK	2.70	2327	2327	215	215	172	206	202	1.85	1.45	27.8	6	5 300	24.8	1.48	8		
N	134	General Fill Area	-	Blended CLAY/ROCK	2.70	2327	2327	181	215	215	215	207	1.85	1.42	30.8	4	4 300	21.4	1.53	11		
N	135	General Fill Area	-	Blended CLAY/ROCK	2.70	2327	2327	215	215	199	187	204	1.83	1.38	32.6	4	4 300	23.4	1.48	11		
N	136	Shear Key 1st Grid	7.1	Blended CLAY/ROCK	2.70	2327	2327	199	169	181	193	186	1.92	1.42	35.4	-3	3 300	49.6	1.28	-11		
N	137	Shear Key 1st Grid	7.2	Blended CLAY/ROCK	2.70	2327	2327	190	203	199	184	194	1.87	1.42	31.6	3	3 300	47.7	1.26	-7		
N	138	Shear Key 1st Grid	7.2	Blended CLAY/ROCK	2.70	2327	2327	141	169	215	215	185	1.81	1.35	33.9	4	4 300	23.2	1.47	12		
7/04/2022 N	139	Shear Key Fill Area	Grid 5	Blended CLAY/ROCK	2.70	2327	2327	172	193	203	215	196	1.78	1.32	34.5	5	5 300	28.7	1.38	9		
N	140	Shear Key Fill Area	Grid 4	Blended CLAY/ROCK	2.70	2327	2327	215	215	172	206	202	1.75	1.26	38.5	4	4 300	31.5	1.33	9		
N	41	Shear Key Fill Area	Grid 5	Blended CLAY/ROCK	2.70	2327	2327	193	184	187	199	191	1.73	1.22	41.2	4	4 300	30.7	1.32	10		
N	142	Shear Key Fill Area	Grid 4	Blended CLAY/ROCK	2.70	2327	2327	178	169	98	209	164	1.84	1.39	32.7	3	3 300	28.5	1.43	6		
6/04/2022 N	143	Shear Key Grid 2	-	Blended CLAY/ROCK	2.70	2327	2327	215	178	150	160	176	1.83	1.31	39.6	(0 300	34.1	1.36	3		
N	144	Shear Key Grid 2	-	Blended CLAY/ROCK	2.70	2327	2327	166	187	181	199	183	1.87	1.35	38.5	-2	2 300	36.8	1.37	-1		
	145	Shear Key Grid 2	-	Blended CLAY/ROCK	2.70	2327	2327	172	181		184	181	1.85	1.34		(500			1		
	146	Lot 18	-	Blended CLAY/ROCK	2.70	2327	2327	153	144	117	141	139	1.73	1.15						6		
	147	Lot 20	-	Blended CLAY/ROCK	2.70	2327	2327	215	215		196	206	1.83	1.33		(6		
	148	Lot 19	-	Blended CLAY/ROCK	2.70	2327	2327	215	181		193	198	1.77	1.25		1				7		
	149	Shear Key Lot 18	Grid 6	Blended CLAY/ROCK	2.70	2327	2327	158	215		184	183	1.76	1.24		2				6		
	150	Shear Key Lot 19	Grid 6	Blended CLAY/ROCK	2.70	2327	2327	193	190		163	182	1.76	1.27		4	4 300		1.34	9		
	151	Shear Key Lot 19	Grid 6	Blended CLAY/ROCK	2.70	2327	2327	107	172		187	162	1.67	1.13		4	4 300		1.25	12		
3/05/2022 N		Lot 26	-	Blended CLAY/ROCK	2.70	2327	2327	215	215		104	187	1.81	1.30		1	1 300			5		
	153	Lot 25	-	Blended CLAY/ROCK	2.70	2327	2327	215	215	147	193	193	1.85	1.32		-1	1 300	-	_	0	ios soor	aaraditati
	ould only b	be reproduced in full.											** Gauge Wet I	Densities outsid	ie of the calibrat	ea range of 1.7!	54 to 2.611 t/m³	are not accredit	ed and are outs	ide the laborator	ies scope of a	accreditation.
Created By:		JLM		Date:	1/04/2022																	
Checked By:		RS		Date:	26/07/2022	2																
Authorised Sig	natory:	JLM		Date:	27/07/2022	2															Page:	1 of 2

AKL2019-0182LAC Rev.0

Milldale 332 Wainui Road

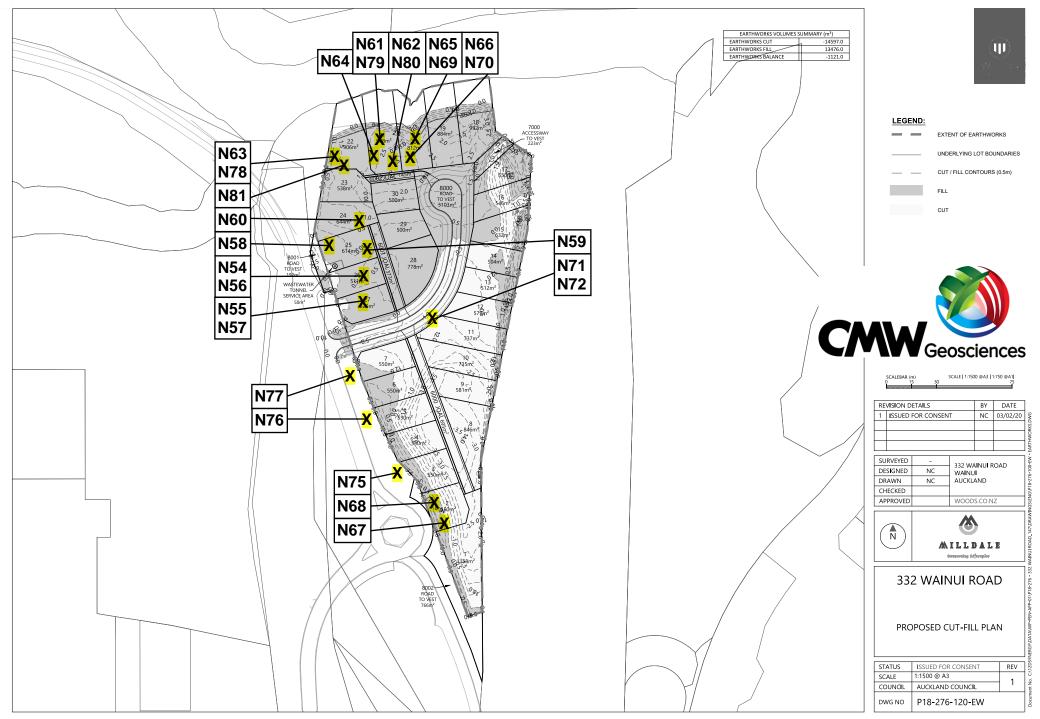
26/07/2022



CM	N Geosci	LF11 Rev.15 Soil Field	d Density NDM D	irect Tra	nsmis	sion w	ith V	SS Re	port (Cohe	sive S	oils)		Auckland Labo CMW Geotecl 11/63, Arrenv PO Box 30020 Phone: +64 (0	nnical NZ Limit vay Drive, Rose 16, Albany, Auc	edale, NZ 0632				
roject:		332 Wainui Road												Test Method	ds:	Notes:	Solid Densit	v:		Assumed
roject No:		AKL2019-0182															Solid Densit	-	e:	N/A
ocation:		Wainui Road												NZS 4407 20	15 Test 3.1 (>	Testing Loca	-		, CMW Field Staff
eport No:		AKL2019-0182LAD Rev.0												NZS 4407 20			-		-	dered for endorsed
eport Date:		14/05/2022												NZGS:Augus			testing			
lient:		Fulton Hogan Land Development Limited															(1) Blade size	of 19mm use	d.	
lient Address:		PO Box 501, Silverdale 0944													PCCREDITED	accredite scope of t	is indicated as not ad are outside the the laboratory's trion			ts marked * are not accredit e the scope of the laborato accreditation
					Var	ie ID	lı	n-situ Va	ne Shear	Strengt	ns			Fie	eld and Labora	tory Testing D	Data	1		
ate Sampled	ample No.	Test Location*	Soil Description*	Solid Density (t/m ³) *	Head #	Blade #	Test 1 (kPa)	Test 2 (kPa)	Test 3 (kPa)	Test 4 (kPa)	Ave.	Gauge Wet Density (t/m³) **	Gauge Dry Density (t/m ³)	Gauge Water Content (%)	Gauge Air Voids (%)	Gauge Probe Depth (mm)		Oven Dry Density (t/m ³)	Oven Calculated Air Voids (%) *	Comments
28/04/2022	154	Lot 26	Blended CLAY/ROCK	2.70	2327	2327	83	95	102	126	102	1.77	1.23	43.2	1	300	39.6	1.27	3	
r	155	Lot 27	Blended CLAY/ROCK	2.70	2327	2327	101	141	144	147	133	1.81	1.28	41.2	0	300	38.4	1.31	2	
29/04/2022	156	Lot 26	Blended CLAY/ROCK	2.70	2327	2327	144	153	169	156	156	1.82	1.28	42.1	-1	300	39.6	1.30	0	
r	157	Lot 27	Blended CLAY/ROCK	2.70	2327	2327	141	144	156	153	149	1.80	1.26	43.5	-1	300	39.7	1.29	1	
6/05/2022 1	158	Lot 25	Blended CLAY/ROCK	2.70	2327	2327	172	187	215	215	197	1.71	1.15	48.1	2	300	41.7	1.20	5	
1	159	Lot 24	Blended CLAY/ROCK	2.70	2327	2327	175	215	206	181	194	1.71	1.17	46.5	3	300	40.9	1.21	6	
1	160	Lot 25	Blended CLAY/ROCK	2.70	2327	2327	215	215	169	209	202	1.85	1.29	43.5	-4	300	44.1	1.28	-4	
14/05/2022	V61	Lot 21	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	203	212	1.81	1.30	38.5	2	300	39.7	1.29	1	
r	N62	Lot 21	Blended CLAY/ROCK	2.70	2327	2327	215	196	209	212	208	1.81	1.30	39.8	0	300	39.1	1.30	1	
13/05/2022 1	N63	Lot 22	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	206	213	1.73	1.22	42.3	4	300	36.7	1.27	7	
r	164	Lot 21	Blended CLAY/ROCK	2.70	2327	2327	215	215	181	199	203	1.80	1.33	35.4	4	300	33.2	1.35	5	
24/05/2022	N65	Lot 19, 5th Grid, Gully Backfill	Blended CLAY/ROCK	2.70	2327	2327	206	215	215	215	213	1.74	1.23	41.2	3	300	39.0	1.25	5	
r	166	Lot 20 Gully Backfill	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.79	1.32	35.7	4	300	38.9	1.29	2	
25/05/2022	N67	Refer to Site Plan	Blended CLAY/ROCK	2.70	2327	2327	181	193	215	215	201	1.64	1.16	41.9	9	300	34.9	1.22	12	
r	168	Refer to Site Plan	Blended CLAY/ROCK	2.70	2327	2327	169	160	163	184	169	1.63	1.17	40.2	10	300	33.8	1.22	13	
17/05/2022	169	Lot 20, 3rd Grid in Gully	Limed CLAY	2.70	2327	2327	160	169	153	147	157	1.65	1.05	56.8	1	300	51.4	1.09	4	
1	170	Lot 20, 3rd Grid in Gully	Limed CLAY	2.70	2327	2327	150	172	156	166	161	1.65	1.06	56.3	1	300	50.7	1.09	4	
22/06/2022 1	171	1/9-1/10, 2m to 1/9, 0.4 BFSL	Blended CLAY/ROCK	2.70	2327	2327	46	52	46	46	48	1.64	1.02	59.9	1	300	67.9	0.97	-2	
	172	1/9-1/10. 0.6m to 1/9, at FSL	Blended CLAY/ROCK	2.70	2327	2327	31	49	64	28	43	1.61	1.01	59.2	3			0.99	2	
29/08/2022 1		Roadbox Undercut Backfill CH10	Blended CLAY/ROCK	2.70	2327	2327	153	129	184	150	154	1.82	1.23	47.9	-4			1.22	-5	
	174	Roadbox Undercut Backfill CH5, 0.5m BSG	Blended CLAY/ROCK	2.70	2327	2327	153	156	184	138	158	1.88	1.39	35.2	0			1.29	-6	
1/09/2022		Berm Backfill	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	156	200	1.75	1.32	32.5	8			1.37	12	
	176	Berm Backfill	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.82	1.38	31.6	5			1.41	7	
	177	Berm Backfill	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	160	201	1.78	1.33	34.2	5			1.39	9	
9/09/2022 1		Refer to Site Plan	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	175	205	1.81	1.34	35.5	3			1.35	4	
	179	Refer to Site Plan	Blended CLAY/ROCK	2.70	2327	2327	215	215	172	190	198	1.80	1.34	34.1	5			1.35	6	
	180	Refer to Site Plan	Blended CLAY/ROCK	2.70	2327	2327	215	215	181	206	204	1.86	1.39	33.8	2			1.35	0	
	v81 ould only l	Refer to Site Plan De reproduced in full.	Blended CLAY/ROCK	2.70	2327	2327	215	215	215	215	215	1.80 ** Gauge Wet	1.32 Densities outsid	36.2 e of the calibrate	3 ed range of 1.75	300 4 to 2.611 t/m ³		1.34 ed and are outsi	4 ide the laborator	ies scope of accreditation.
·	, .																			
reated By:		PM	Date:		05/2022															
necked By:		RS	Date:		10/2022															
uthorised Sig	natory:	JLM	Date:	28/	10/2022															Page: 1 of 3

AKL2019-0182LAD Rev.0

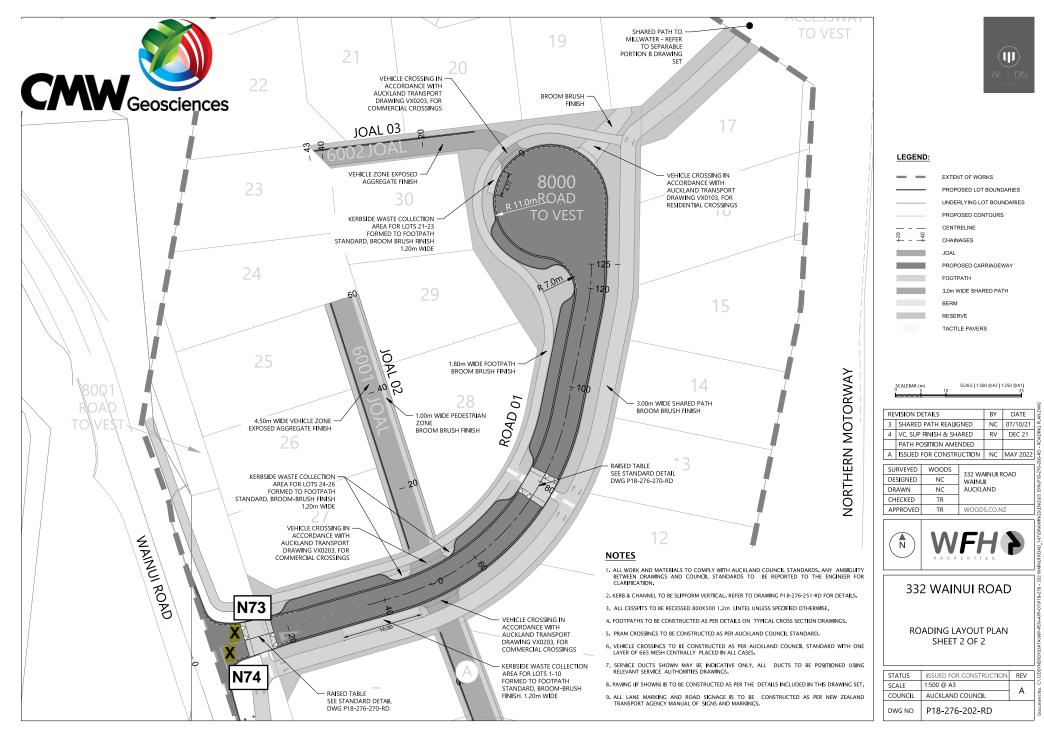
14/05/2022



AKL2019-0182LAD Rev.0

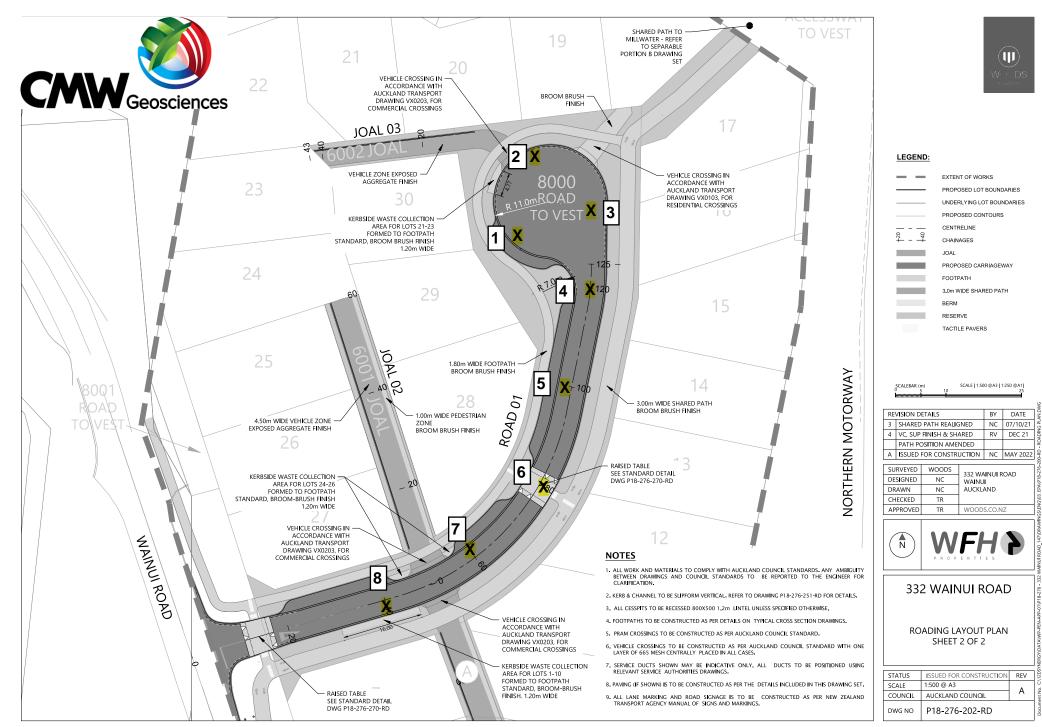
332 Wainui Road

14/05/2022

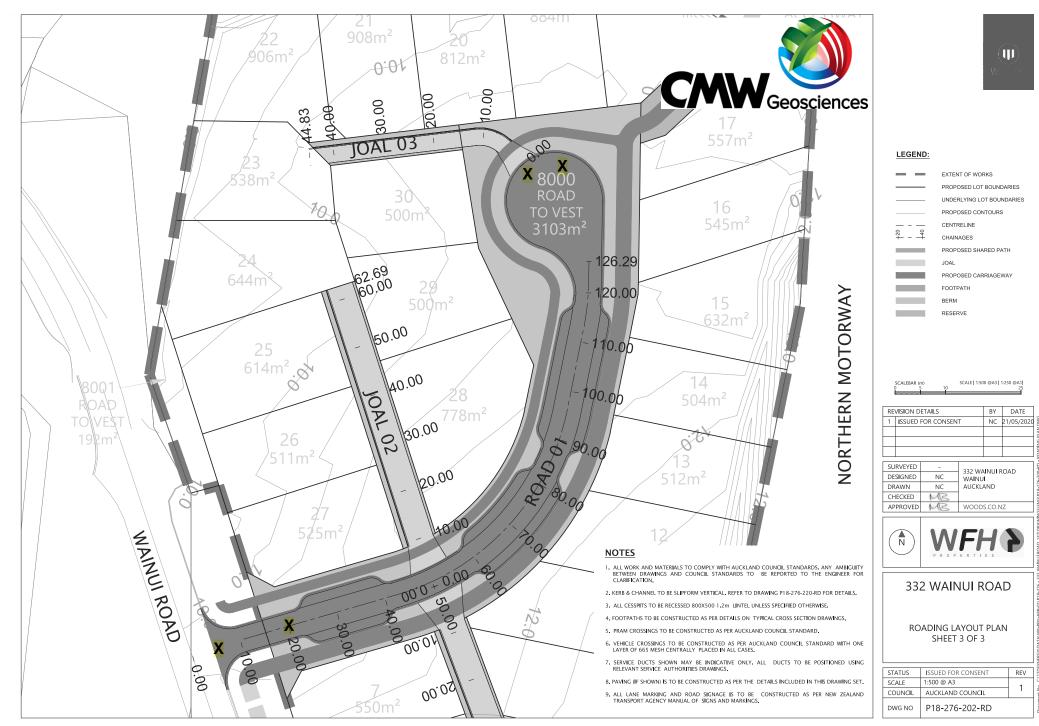


CMWGee	Disciences		LF14 Rev.14	Dynam		Penetra 5 4402: 1988 Test	tion (DC 5.5.2	P) Test I	Report	
Project: Project No: Location: Report No:		Milldale 332 Wainu AKL2019-0182 Wainui Road AKL2019-0182LAE I				11/63, Arrenwa	nical NZ Limited ay Drive, Roseda , Albany, Auckla			
Test Date:		24/08/2022				lesting Locatio	ns Selected By:		CMW Field Staf	ſſ
Tested By:		SDM				CCREDI				
Client:		Fulton Hogan Land	Development Limite	ed			Test results inc accredited and scope of the l	licated as not e outside the		R Values are not outside the scope of
Client Address:		PO Box 501, Silverd	ale 0944			TS HAG LABO	accreditation		the laboratory	's accreditation
CBR Test Calculation:		Austroads (2010) (f	ine grained cohesive	2)						
Test No		1		2		3		4		5
Test Location	Cul c	le sac	Cul c	le sac	Culo	de sac	Roa	ad 1	Roa	ad 1
Chainage & Offset			Refer to	Site Plan			СН	120	СН	100
Material & Layer					SG-CLAY Pr	re Stabalized				
Depth (mm)	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*
0 - 100	0	0	0	0	1	2	1	2	2	4
100 - 200	3	6	2	4	3	6	3	6	5	10
200 - 300	5	10	1	2	3	6	5	10	8	18
300 - 400	13	20+	0	0	3	6	6	13	7	15
400 - 500			3	6	2	4	5	10	4	8
500 - 600			5	10	3	6	4	8	3	6
600 - 700			4	8	10	20+	3	6	4	8
700 - 800			2	4	7	15	2	4	3	6
800 - 900			4	8	7	15	4	8	3	6
900 - 1000			8	18	6	13	3	6	3	6
Test No		6		7		8				
Test Location	Roa	ad 1	Roa	ad 1	Ro	ad 1				
Chainage & Offset	CH	180	CH	160	CH40 1.2	2m R of CL				
Material & Layer			SG-CLAY Pr	e Stabalized						
Depth	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*
0 - 100	2	4	5	10	2	4				
100 - 200	2	4	4	8	6	13				
200 - 300	2	4	4	8	3	6				
300 - 400	1	2	9	20	6	13				
400 - 500	2	4	8	18	7	15				
500 - 600	3	6	5	10	3	6				
600 - 700	3	6	3	6	5	10				
700 - 800	3	6	4	8	5	10				
800 - 900	2	4	4	8	6	13				
900 - 1000	2	4	3	6	4	8			 	
Created by:	by: JLM Da			Date:	26/08/2022		* Equivalent CBF	R values are taken from	ly be reproduced i m Fig 5.3, Austroads Gu Design, Austroads 2010	uide to Pavement
Checked by:	RS			Date:	14/10/2022		. comology, rait 2.		ied soils only.	
Authorised Signatory:	JLM			Date:	28/10/2022				Page 1 of 2	

24/08/2022



CMW	sciences		LF14 Rev.14	Dynam		Penetra		P) Test F	Report	
Project:		Milldale 332 Wainu	ii Road			Auckland Labor	atory			
Project No:		AKL2019-0182				CMW Geotech				
Location:		Wainui Road					iy Drive, Roseda , Albany, Auckla			
Report No:		AKL2019-0182LAF F	Rev.0			Phone: +64 (09) 4144 632			
Test Date:		25/08/2022				Testing Locatio	ns Selected By:		CMW Field Staf	f
		SDM				Testing Locatio	in beleeted by:			•
Tested By:						CCREE	Tre.			
Client:		Fulton Hogan Land	Development Limite	ed			Test results accredited	ndicated as not are outside the e laboratory's	accredited and are	R Values are not outside the scope of
Client Address:		PO Box 501, Silverd	ale, 0944			ESTING LAN	of ATO accreditati	e laboratory's on	the laboratory	's accreditation
CBR Test Calculation:		Austroads (2010) (f	ine grained cohesive	2)						
Test No		1		2		3		4		
Test Location	Cul de sao	soft spots	Cul de sac	soft spots	Ro	ad 1	Roa	ad 1		
Chainage & Offset		-		-	CH20 1.	2m L of C	CH5 1.2	m R of C		
Material & Layer	SG-CLAY	' Pre Stab	SG-CLAY	Pre Stab	SG-CLAY	Pre Stab	SG-CLAY	Pre Stab		
Depth (mm)	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*
0 - 100	2	4	0	0	2	4	0	0		
100 - 200	3	6	1	2	2	4	3	6		
200 - 300	2	4	4	8	1	2	3	6		
300 - 400	4	8	6	13	2	4	3	6		
400 - 500	4	8	4	8	2	4	2	4		
500 - 600	9	20	5	10	3	6	2	4		
600 - 700	10	20+	5	10	4	8	2	4		
700 - 800			6	13	2	4	3	6		
800 - 900			4	8	5	10	1	2		
900 - 1000			5	10	5	10	1	2		
Test No						•				
Test Location										
Chainage & Offset										
Material & Layer										
Depth	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*
0 - 100										
100 - 200										
200 - 300										
300 - 400										
400 - 500										
500 - 600										
600 - 700										
700 - 800										
800 - 900										
900 - 1000										
							This	report should on	ly be reproduced i	n full
Created by:	JLM			Date:	29/08/2022			Pavement Structural D	n Fig 5.3, Austroads Gu Design, Austroads 2010	
Checked by:	RS			Date:	14/10/2022			to fine grain	ed soils only.	
Authorised Signatory:	JLM			Date:	28/10/2022				Page 1 of 2	

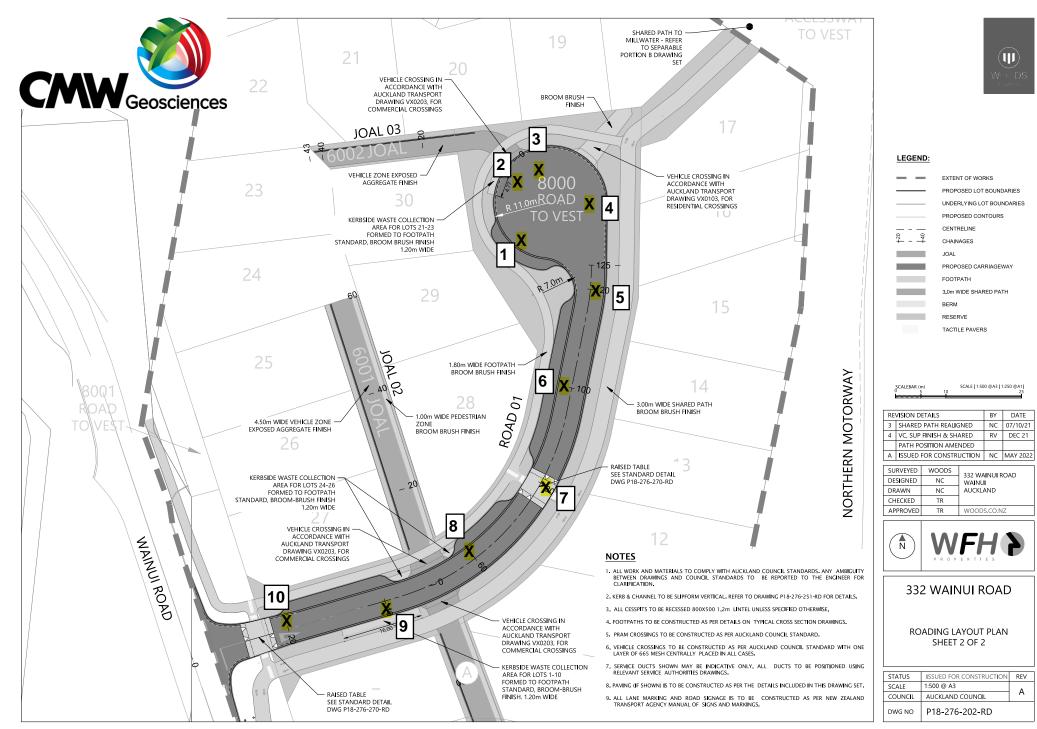


Project: Project No: Location:		Milldale 332 Wainu			NZS	4402: 1988 Test (5.5.2			
-			i Road							
-		AKL2019-0182				Auckland Labor CMW Geotechi				
		Wainui Road					ay Drive, Rosedal , Albany, Aucklar			
Down and No.		AKL2019-0182LAG I	Roy 0			Phone: +64 (09		10,112 07 52		
Report No:			Nev.0							
Test Date:		29/08/2022				Testing Locatio	ns Selected By:		CMW Field Staf	f
Tested By:		SDM				CCREDIT	2 1			
Client:		Fulton Hogan Land	Development Limite	ed .			Test results ind accredited are scope of the k	icated as not a outside the		R Values are not outside the scope of
Client Address:		PO Box 501, Silverd	ale, 0944			TESTING LABOR	accreditation	and doing a		's accreditation
CBR Test Calculation:		Austroads (2010) (fi	ine grained cohesive	2)						
Test No		1	:	2		3		4		5
Test Location	Cul D	e Sac	Cul D	e Sac	Cul D	De Sac	Cul D	e Sac	Roa	ad 1
Chainage & Offset						-			СН	120
Material & Layer	Subg	rade	Sube	grade	Sub	grade	Subg	rade	Sub	grade
Depth (mm)	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*
0 - 100	10	20+	9	20	7	15	9	20	6	13
100 - 200	7	15	7	15	5	10	9	20	6	13
200 - 300	5	10	5	10	3	6	5	10	3	6
300 - 400	6	13	4	8	3	6	3	6	3	6
400 - 500	5	10	9	20	3	6	4	8	3	6
500 - 600	5	10	10+	20+	3	6	2	4	3	6
600 - 700	5	10			3	6	3	6	2	4
700 - 800	4	8			3	6	3	6	2	4
800 - 900	5	10			3	6	5	10	3	6
900 - 1000	4	8			3	6	3	6	4	8
Test No	(5		7		8	9	9	1	10
Test Location	Roa	ad 1	Roa	ad 1	Ro	ad 1	Roa	ad 1	Roa	ad 1
Chainage & Offset	СН	100	СН	80	CH	1 60	СН	40	CH	120
Material & Layer	Subg	rade	Subg	grade	Sub	grade	Subg	rade	Sub	grade
Depth	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*	Blow Count	Equiv CBR*
0 - 100	3	6	4	8	9	20	5	10	8	18
100 - 200	3	6	4	8	7	15	9	20	5	10
200 - 300	5	10	2	4	4	8	8	18	4	8
300 - 400	3	6	3	6	5	10	5	10	4	8
400 - 500	4	8	3	6	4	8	2	4	4	8
500 - 600 600 - 700	3	6 8	2	4	5	10 6	3	6	4	8
700 - 800	3	6	3	2	5	10	3	13 6	2	8
800 - 900	3	6	1	2	4	8	3	6	4	8
900 - 1000	4	8	2	4	4	8	4	8	4	8
500 1000	Ŧ	3	<u> </u>	-	-				y be reproduced i	
Checked by:	RS			Date: Date:	8/09/2022			Pavement Structural D	n Fig 5.3, Austroads Gu Design, Austroads 2010 Ied soils only.	
Authorised Signatory:	RS			Date:	14/10/2022 28/10/2022				Page 1 of 2	

AKL2019-0182LAG Rev.0

322 Wainui Road

29/08/2022



Great Peop		osciences	LF11 Rev.17	Soil Field	Density NDM D	irect Tra	insmis	sion w	vith V	SS Re	port (Cohe	sive S	ioils)		11/63, Arrenv	hnical NZ Limit vay Drive, Rose 6, Albany, Auc	edale, NZ 0632				
Project:		332 Wainui Roa	d													Test Metho	ds:	Notes:	Solid Densit	y:		Assumed
roject No:		AKL2019-0182																	Solid Densit		e:	N/A
ocation:		Wainui Road														NZS 4407 20	15 Test 3.1 0	>	Testing Loca			, CMW Field Staff
Report No:		AKL2019-0182L4	AH Rev.0													NZS 4407 20			•			lered for endorsed
leport Date:		17/02/2023														NZGS:Augus	t 2001		testing			
lient:		Fulton Hogan La	nd Development	Limited															 Blade size 	of 19mm use	d.	
Client Address	:	PO Box 501, Silv	erdale 0944														FITING LABO	All tes have l accor labor	ats reported herein been performed in dance with the atory's scope of ditation			s marked * are not accredite e the scope of the laboratoric accreditation
			Test Location*				Van	e ID	h	n-situ Va	ne Shear	Strength	5			Fie	eld and Labora	atory Testing I	Data			
Date Sampled	Sample No.	Test	Area	RL/Depth	Soil Description*	Solid Density (t/m ³) *	Head #	Blade #	Test 1 (kPa)	Test 2 (kPa)	Test 3 (kPa)	Test 4 (kPa)	Ave.	Gauge Wet Density (t/m³) **	Gauge Dry Density (t/m³)	Gauge Water Content (%)	Gauge Air Voids (%)	Gauge Probe Depth (mm)		Oven Dry Density (t/m ³)	Oven Calculated Air Voids (%) *	Comments
22/10/2022	N82	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	187	184	190	153	179	1.86	1.42	31.1	3	300	30.6	1.43	4	
	N83	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	199	190	215	98	176	1.86	1.40	32.5	2	300	28.0	1.45	6	
	N84	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	215	215	187	181	200	1.85	1.39	33.3	2	300	29.5	1.43	5	
	N85	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	184	215	215	215	207	1.95	1.49	30.4	-1	300	27.4	1.53	1	
	N86	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	172	203	215	215	201	1.95	1.52	27.9	1	300	28.4	1.52	1	
25/10/2022	N87	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	190	114	150	212	167	1.80	1.30	38.2	2	300	28.4	1.40	8	
26/10/2022	N88	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	141	160	172	184	164	1.75	1.23	41.9	3	300	36.0	1.28	6	
	N89	Pond Backfill		-	Blended Clay/Rock	2.70	2327	2327	138	160	144	150	148	1.73	1.18	46.6	1	300	35.1	1.28	8	
9/09/2022	N90	A8-A9		at FSL	Blended Clay/Rock	2.70	2327	2327	83	74	71	77	76									No Sample Taken
	N91	A11-A10		at FSL	Blended Clay/Rock	2.70	2327	2327	215	199	166	129	177	1.78			3					
	N92	A11-A12		-	Blended Clay/Rock	2.70	2327	2327	215	215	215	215	215	1.74			4	300				
	N93	A12-A13		-	Blended Clay/Rock	2.70	2327	2327	215	215	215	215	215	1.76	1.25	40.1	3	300	30.2	1.35	9	
	N94	A14-A15		-	Blended Clay/Rock	2.70	2327	2327	52	71	58	64	61									No Sample Taken
27/10/2022		Refer to Site Pla		-	Blended Clay/Rock	2.70	2327	2327	215	215	156	172	190	1.77	1.28	39.0	3			1.26	2	
	N96	Refer to Site Pla		-	Blended Clay/Rock	2.70	2327	2327	138	160	132	150	145	1.80	1.40	28.3	8			1.39		
	N97	Refer to Site Pla Lot 75	n	-	Blended Clay/Rock	2.70	2327	2327	160	147	166	172	161	1.80	1.25		-2 2			1.30		
2/11/2022	N98 N99	Lot 75 Refer to Site Pla	n	-	Blended Clay/Rock Blended Clay/Rock	2.70 2.70	2327 2327	2327 2327	181 104	199 110	215 215	215 110	203 135	1.77	1.26	40.5	2	300	34.0	1.32	6	No Sample Taken
	N99 N100	Refer to Site Pla		-	Blended Clay/Rock	2.70	2327	2327	83	110	80	110	135 97									No Sample Taken
5/11/2022		Lot 15		-	Blended Clay/Rock	2.70	3449	3449	231	231	231	224	229	1.78	1.28	38.7	3	300	35.3	1.31	5	
	N101	Lot 14			Blended Clay/Rock	2.70	3449	3449	231	231	205	214	220	1.78	1.28	39.9	2			1.31	3	
7/11/2022		Lot 10		-	Blended Clay/Rock	2.70	3449	3449	231	231	231	205	225	1.75	1.39	33.0	2				1	
	N104	Lot 11		-	Blended Clay/Rock	2.70	3449	3449	231	231	178	188	207	1.86	1.38	34.8	1	300		1.38	0	
	N105	Lot 12		-	Blended Clay/Rock	2.70	3449	3449	231	231			231+	1.83	1.35		2			1.36	2	
his report sh	ould only l	be reproduced	in full.											** Gauge Wet	Densities outsid	e of the calibrate	ed range of 1.75	54 to 2.611 t/m ³	are not accredit	ed and are outs	ide the laborato	ries scope of accreditation.
Created By:					Date:	1/11/2																
Checked By:					Date:	17/02/																
uthorised Si	gnatory (K ⁻	ΓP):	JLM		Date:	17/02/	/2023															Page: 1 of 3

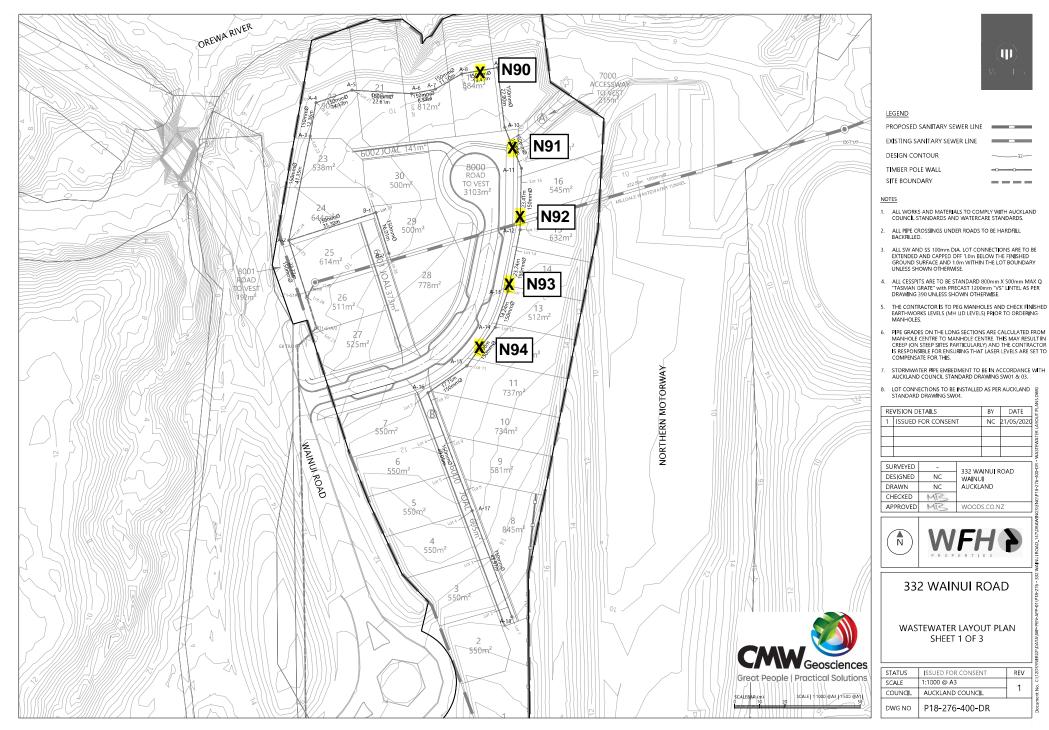
AKL2019-0182LAH Rev.0

332 Wainui Road

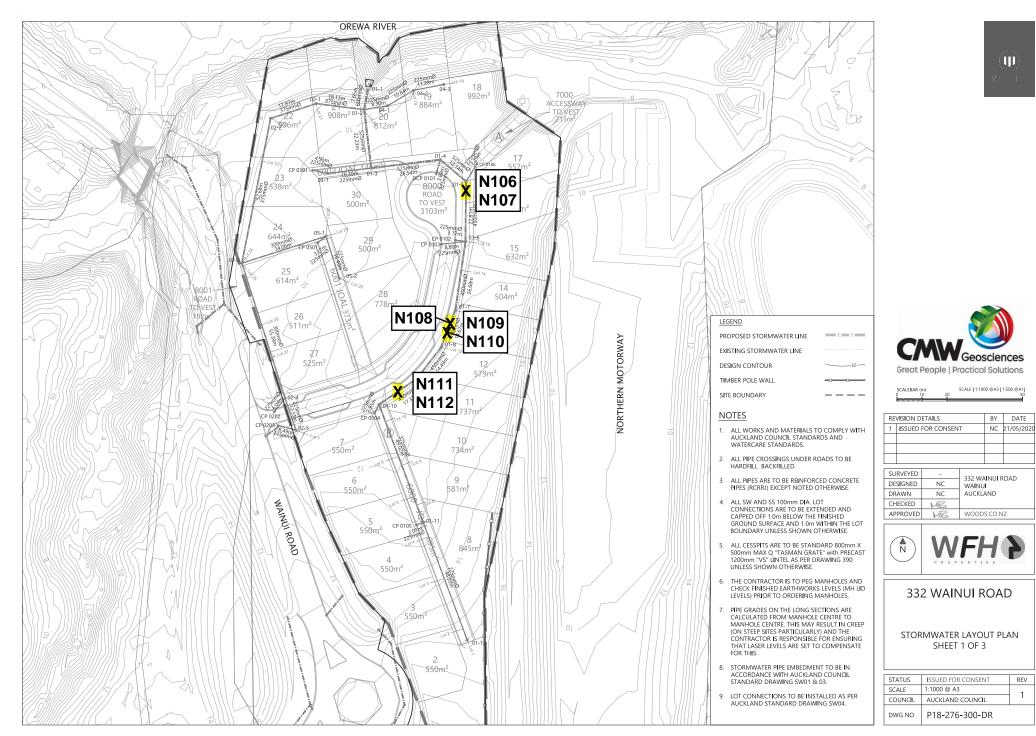
17/02/2023

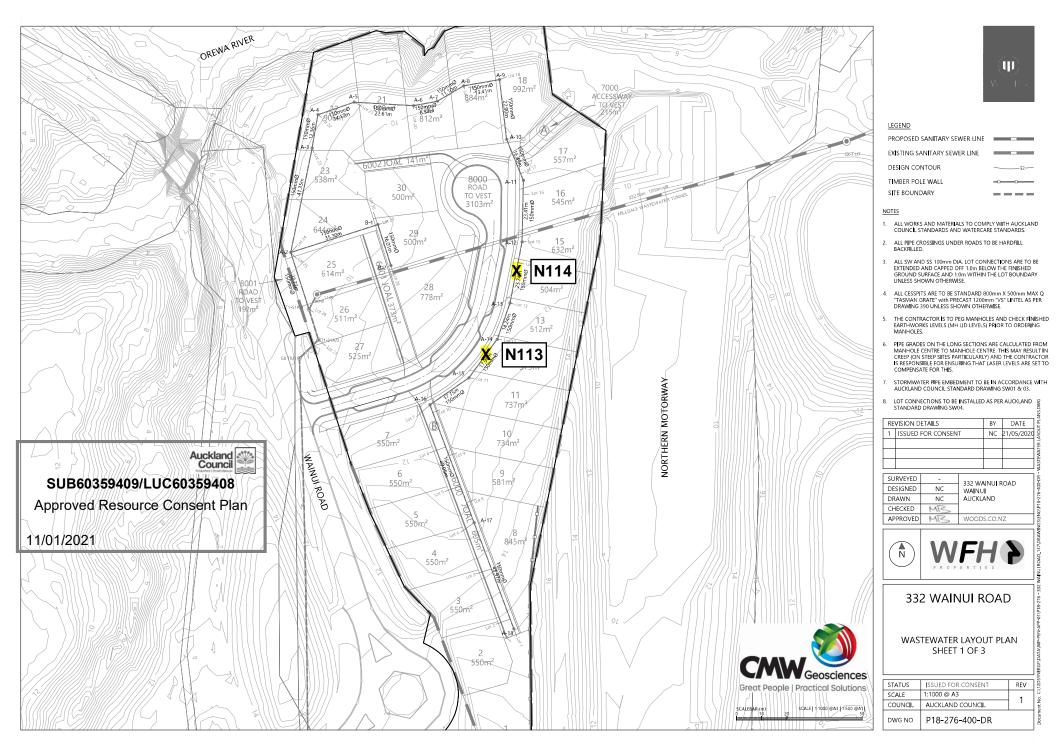




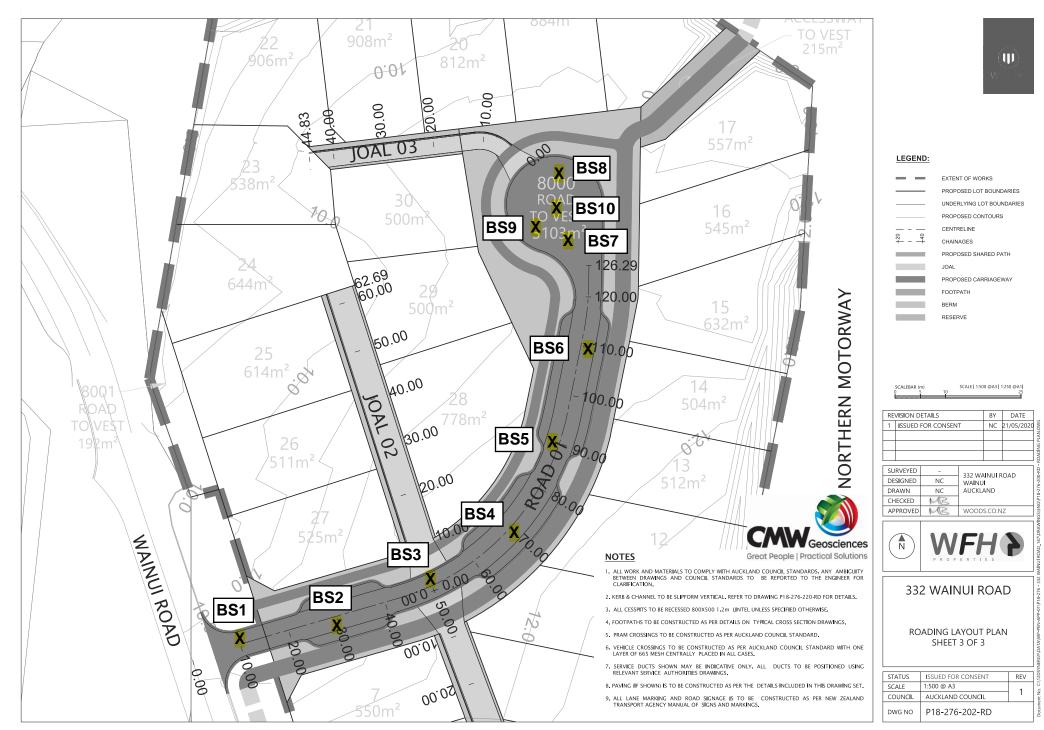


Great Peop		sciences	LF11 Rev.17	Soil Field	Density NDM D	irect Tra	nsmis	sion w	vith VS	SS Re	port (Cohe	esive S	Soils)			hnical NZ Limit vay Drive, Rose 6, Albany, Auc	edale, NZ 0632				
Project:		332 Wainui Road	d													Test Metho	ds:	Notes:	Solid Density	<i>/</i> :		Assumed
Project No:		AKL2019-0182																	Solid Density	Data Source	e:	N/A
Location:		Wainui Road														NZS 4407 20	15 Test 3.1 0		Testing Loca			, CMW Field Staff
Report No:		AKL2019-0182LA	l Rev.0													NZS 4407 20	15 Test 4.2		-			ered for endorsed
Report Date:		22/03/2023														NZGS:Augus			testing			
Client:		Fulton Hogan La	nd Development	Limited															 Blade size 	of 19mm used	d.	
Client Address	:	PO Box 501, Silve	erdale 0944														FILM G LABO	All test have b accord	s reported herein een performed in lance with the tory's scope of litation			marked * are not accredited the scope of the laboratories accreditation
			Test Location*				Van	ie ID	In	n-situ Va	ne Shear	Strengtl	ıs			Fie	eld and Labora	tory Testing D	ata			
Date Sampled	Sample No.	Test	Site	RL/Details	Soil Description*	Solid Density (t/m³) *	Head #	Blade #	Test 1 (kPa)	Test 2 (kPa)	Test 3 (kPa)	Test 4 (kPa)	Ave.	Gauge Wet Density (t/m³) **	Gauge Dry Density (t/m³)	Gauge Water Content (%)	Gauge Air Voids (%)	Gauge Probe Depth (mm)		Oven Dry Density (t/m ³)	Oven Calculated Air Voids (%) *	Comments
28/11/2022	N106	01/5-01/6, 4m-0	1/5	0.3m BFSL	Blended Clay/Rock	2.70	2327	2327	170	194	127	164	164	1.84	1.34	36.5	1	300	28.9	1.42	6	
	N107	01/5-01/6, 5m-0	1/5	at FSL	Blended Clay/Rock	2.70	2327	2327	157	173	142	139	153	1.85	1.32	40.2	-2	300	31.4	1.40	4	
	N108	01/7-01/8, 7m-0	1/7	0.3m BFSL	Blended Clay/Rock	2.70	2327	2327	UTP	UTP	UTP	UTP	UTP	1.69	1.12	50.2	2	300	44.1	1.17	5	
29/11/2022	N109	01/7-01/8, 8m-0	1/7	0.3m BFSL	Blended Clay/Rock	2.70	2327	2327	99	201	185	167	163	1.73	1.22	41.0	4	300	33.7	1.29	9	
	N110	01-7-01/8, 9m-0	1/7	at FSL	Blended Clay/Rock	2.70	2327	2327	167	198	167	179	178	1.83	1.35	35.5	2	300	30.4	1.41	5	
	N111	01/9-01/10, 7m-	01/10	0.3m BFSL	Blended Clay/Rock	2.70	2327	2327	160	160	173	142	159	1.85	1.34	38.3	-1	300	36.6	1.35	0	
	N112	01/9-01/10, 6m-	01/10	at FSL	Blended Clay/Rock	2.70	2327	2327	93	157	104	164	130	1.86	1.36	36.4	0	300	37.2	1.36	-1	
19/12/2022	N113	A14-A15, 10m-A	14	at FSL	Blended Clay/Rock	2.70	2327	2327	105	111	157	139	128	1.80	1.29	39.7	1	300	39.1	1.30	1	
	N114	A12-A13, 10m-A	12	at FSL	Blended Clay/Rock	2.70	2327	2327	99	130	142	117	122	1.79	1.28	40.0	1	300	37.0	1.31	3	
This report sh Created By:	,	e reproduced	in full.		Date:	1/1	12/2022	<u> </u>	<u> </u>					** Gauge Wet [Densities outsid	l e of the calibrate	ed range of 1.75	 4 to 2.611 t/m³	are not accredite	ed and are outsi	de the laboratori	es scope of accreditation.
					Date:)3/2023															
Checked By:																						

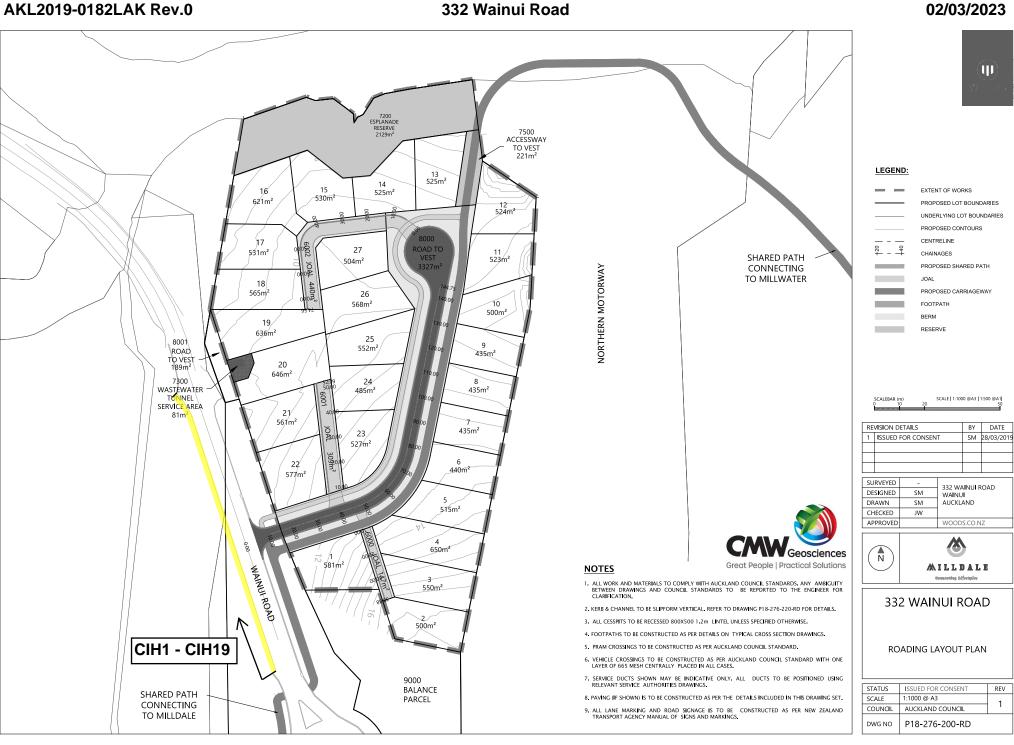




C M Great Peo	ple Practice	sciences	.F12 Rev.16 Aggreg	ate Fielo	d Density NDI	M - Backscatter Report					Auckland Laborator CMW Geotechnical 11/63, Arrenway D PO Box 300206, Alt Phone: +64 (09) 41	, NZ Limited rive, Rosedale, NZ pany, Auckland, NZ			
Project:		332 Wainui Road									Test Methods:		Notes:		
Project No:		AKL2019-0182											Solid Density:		Assumed
Location:		Wainui Road									NZS 4407:2015 T	est 3.1 ◊	Soild Density Da	ta Source:	N/A
Report No:		AKL2019-0182LAJ	Rev.0								NZS 4407:2015 T	est 4.3	Testing Location	s Selected By:	CMW Field Staff
Report Date:		21/12/2022									♦ Only samples <	2.0mm will be co	nsidered for endo	rsed testing	
Client:		Fulton Hogan Lan	d Development Limited									PCCREDITEO			Measurements marked *
Client Address	5:	PO Box 501, Silver	dale 0944										All tests reported herein have been performed in accordance with the laboratory's scope of accreditation		are not accredited and are outside the laboratory's scope of accreditation
		1	Fest Location*			Material Details					Fi	eld and Testing Da	ta		
Date Sampled	Sample No.	Test A	rea RL/Depth	Material*	Quarry	Material Data Source	OMC* (%)		SD* (t/m ³)	Gauge Wet Density (t/m ³) **	Gauge Dry Density (t/m³)	Gauge Water Content (%)	Calculated Compaction (%) *	Calculated Total Voids (%) *	Comments
16/12/2022	BS1	CH10	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.39	2.25	6.0	102	1	7
	BS2	СН30	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.45	2.31	6.2	105	19	5
	BS3	СН50	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.43	2.30	5.7	105	19	5
	BS4	СН70	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.37	2.24	5.9	102	2 17	7
	BS5	СН90	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.44	2.31	5.3	105	5 15	5
	BS6	CH110	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.41	2.28	6.1	L 103	16	5
	BS7	CH130	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.44	2.32	5.0	106	5 14	1
	BS8	CH150	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.39	2.26	5.9	103	1	7
	BS9	CH170	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.38	2.26	5.6	5 103	1	7
	BS10	Cul de Sac Centre	Basecourse	TNZ40	Drury Quarry	Stevenson Report #45195T, Test#225623, Ref#976	5.50	2.20	2.71	2.37	2.25	5.3	3 102	1	7
This report sl	l hould only l	be reproduced i	in full.		1	1		1		** Gauge Wet Densit scope of accreditatio		brated range of 1.754	to 2.611 t/m ³ are not	t accredited and are	outside the laboratories
Created By:					Date:	21/12/20									
Checked By:					Date:	22/03/20									
Authorised S	ignatory (K	TP): J	LM		Date:	22/03/20)23								Page: 1 of 2



Great People Practical Solutions			CT HAMMER			т	
Project:	332 Wainui Road			Auckland Labo	ratory		
Project No:	AKL2019-0182				nical NZ Limite ay Drive, Rosec		
Location:	Wainui Road			PO Box 300206	5, Albany, Auck		
Report No:	AKL2019-0182LAK Rev.0			Phone: +64 (09	9) 4144 632		
Report Date:	2/03/2023			Testing Locatio	ons Selected By	:	CMW Field Staff
Client:	Fulton Hogan Land Development Li	mited					Measurements marked * are not
Client Address:	PO Box 501, Silverdale 0944						accredited and are outside of the scope of the laboratory's accreditation
Test No:	Date Tested:	Test Location*	Impact Hammer No	Material**	Impact Value (IV)**	Inferred ① CBR %	Notes
CIH1	21/02/2023	Wainui Road Widening	CIH05	TNZ40	73	373	
CIH2	21/02/2023	Wainui Road Widening	CIH05	TNZ40	100	700	
СІНЗ	21/02/2023	Wainui Road Widening	CIH05	TNZ40	53	197	
CIH4	21/02/2023	Wainui Road Widening	CIH05	TNZ40	73	373	
CIH5	21/02/2023	Wainui Road Widening	CIH05	TNZ40	44	136	
СІН6	21/02/2023	Wainui Road Widening	CIH05	TNZ40	54	204	
CIH7	21/02/2023	Wainui Road Widening	CIH05	TNZ40	70	343	
CIH8	21/02/2023	Wainui Road Widening	CIH05	TNZ40	60	252	
СІН9	21/02/2023	Wainui Road Widening	CIH05	TNZ40	51	182	
CIH10	21/02/2023	Wainui Road Widening	CIH05	TNZ40	48	161	
CIH11	21/02/2023	Wainui Road Widening	CIH05	TNZ40	37	96	
CIH12	21/02/2023	Wainui Road Widening	CIH05	TNZ40	46	148	
CIH13	21/02/2023	Wainui Road Widening	CIH05	TNZ40	62	269	
CIH14	21/02/2023	Wainui Road Widening	CIH05	TNZ40	54	204	
CIH15	21/02/2023	Wainui Road Widening	CIH05	TNZ40	68	324	
CIH16	21/02/2023	Wainui Road Widening	CIH05	TNZ40	66	305	
CIH17	21/02/2023	Wainui Road Widening	CIH05	TNZ40	74	383	
CIH18	21/02/2023	Wainui Road Widening	CIH05	TNZ40	81	459	
CIH19	21/02/2023	Wainui Road Widening	CIH05	TNZ40	93	605	
** Measurements with a maximu	m particle size > 37.5mm are	outside of the scope of ASTM D5874:20 of the laboratory		pact Values on s	such materials a	are not accredit	ed and are outside of the scope
Created By:	RS	Date:	2/03/2023		This r	eport should or	nly be reproduced in full
Checked By:	RS	Date:	22/03/2023		(1) In	ferred CBR Calo	culation: CBR= IV ² x0.07
Authorised Signatory (KTP):	JLM	Date:	22/03/2023			Page	e 1 of 2



Appendix E: Laboratory Test Data



Project Name :	332 Wainui Road		
		Project No :	22 0001 85
Client :	CMW Geosciences	Page :	1 of 1
Address :	PO Box 300206	Date of Order :	05.11.22
	Albany, Auckland 0754		
		Sample Method :	Hand auger
Attention :	Fletcher Swan	Sample Date :	02.11.22
		Sampled By :	CMW Geosciences

Test Details :

Test performed on : History : Whole Sample Natural

Sample No.	Location	Depth (m)	Cone Penetration (CPL)	Linear Shrinkage (LS)	Natural Water Content (%)
049O	Lot 26	0.5 to 0.8	91	22	38.9
050O	Lot 20	0.5 to 0.9	70	16	33.5
051O	Lot 12	0.5 to 0.10	88	20	55.5
052O	Lot 3	0.5 to 0.11	103	22	62.7

Comments :

Tested By:	RS	Date :	07 to 09.11.22
Calculated By :	RS	Date :	11.11.22
Checked By :	ZH	Date :	11.11.22